# A TSUNAMI FORECAST MODEL FOR ARECIBO, PR

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#### Foreword

Tsunamis have been recognized as a potential hazard to United States coastal communities since the mid-twentieth century, when multiple destructive tsunamis caused damage to the states of Hawaii, Alaska, California, Oregon, and Washington. In response to these events, the United States, under the auspices of the National Oceanic and Atmospheric Administration (NOAA), established the Pacific and Alaska Tsunami Warning Centers, dedicated to protecting United States interests from the threat posed by tsunamis. NOAA also created a tsunami research program at the Pacific Marine Environmental Laboratory (PMEL) to develop improved warning products.

The scale of destruction and unprecedented loss of life following the December 2004 Sumatra tsunami served as the catalyst to refocus efforts in the United States on reducing tsunami vulnerability of coastal communities, and on 20 December 2006, the United States Congress passed the "Tsunami Warning and Education Act" under which education and warning activities were thereafter specified and mandated. A "tsunami forecasting capability based on models and measurements, including tsunami inundation models and maps." is a central component for the protection of United States coastlines from the threat posed by tsunamis. The forecasting capability for each community described in the PMEL Tsunami Forecast Series is the result of collaboration between the National Oceanic and Atmospheric Administration office of Oceanic and Atmospheric Research, National Weather Service, National Ocean Service, National Environmental Satellite Data and Information Service, the University of Washington's Joint Institute for the Study of the Atmosphere and Ocean, National Science Foundation, and United States Geological Survey.

#### Abstract

This study documents the development of a tsunami forecast model for Arecibo, Puerto Rico. The town of Arecibo is located on the Northern coast of the island of Puerto Rico in the Atlantic Ocean. It is particularly exposed to tsunamis originating in the Puerto Rico trench approximately 100 km north of the island. The Puerto Rico Trench separates the North American and Caribbean plates and extends for approximately 1750 km with a width of almost 100 km. Its deepest (Milwaukee Point) is the deepest point outside of the Pacific Ocean.

Since there is no quantitative information about large historical tsunami events for the island of Puerto Rico, it is not possible to use such events for validation of the inundation forecast model for Arecibo. Accuracy of the results is addressed in this study by comparing the solution obtained using the forecast model and that obtained with a higher resolution model for 6 synthetic mega-tsunami scenarios originating in different regions of the Caribbean and Atlantic Ocean. In addition to the mega-tsunami scenarios a more probable Mw=7.5 scenario is also simulated as well as a micro-tsunami triggered by a seismic event in the South Sandwich Islands, located in the South Atlantic.

Results from this study confirm that the Puerto Rico Trench poses the largest tsunami

hazard to the town of Arecibo.

# 1.0 Background and Objectives

The Pacific Marine Environmental Laboratory (PMEL) of the National Oceanic and Atmospheric Administration (NOAA) Center for Tsunami Research (NCTR) has developed a tsunami forecasting capability for operational use by NOAA's two Tsunami Warning Centers located in Hawaii and Alaska (Titov et al. 2005). The system is designed to efficiently provide basin-wide warning of approaching tsunami waves. The system termed Short-term Inundation Forecast of Tsunamis (SIFT) combines real-time tsunami event data with numerical models to produce estimates of tsunami wave arrival times and amplitudes at a coastal community of interest. The SIFT system integrates several key components: deep-ocean, real-time observations of tsunamis, a basin-wide pre-computed propagation database of water level and flow velocities based on potential seismic unit sources, an inversion algorithm to refine the tsunami source based on deep-ocean observations during an event, and optimized tsunami forecast models.

The objective of the present work is to construct a tsunami inundation model for Arecibo, Puerto Rico that can be used by the Tsunami Warning Centers to assess, in real time, the local impact of a tsunami generated anywhere in the Caribbean or Atlantic Ocean.

The most relevant bathymetric feature offshore of Arecibo is the Puerto Rico Trench. The trench is the result of the Caribbean and North American plates sliding past each other and is the deepest point in the Atlantic Ocean. It has the potential for triggering large tsunami events, having generated earthquakes with magnitude larger than 8.0 in the past, such as the 1787 event. At a more local scale, the other relevant bathymetric feature, offshore of Arecibo is the presence of the Arecibo Canyon, a submarine valley that could potentially behave as a tsunami wave-guide.

This report details the development of a high-resolution tsunami forecast model for Arecibo, PR including development of the bathymetric grids, model validation and stability testing with a set of synthetic mega-tsunami events (Mw 9.3). Inundation results from such artificial events are presented in later sections.

# 2.0 Forecast Methodology

A high-resolution inundation model was used as the basis for the operational forecast model to provide an estimate of wave arrival time, height, and inundation immediately following tsunami generation. Tsunami forecast models are run in real time while the tsunami in question is propagating across the open ocean. These models are designed and tested to perform under very stringent time constraints given that time is generally the single limiting factor in saving lives and property. The goal is to maximize the amount of time that an at-risk community has to react to a tsunami threat by providing accurate information quickly. To this end, the tsunami propagation solution in deep water is precomputed in the linear wave regime and used to force the inundation forecast models during the last stage of tsunami propagation and runup.

The tsunami forecast model, based on the Method of Splitting Tsunami (MOST),

emerges as the solution in the SIFT system by modeling real-time tsunamis in minutes SIFT employs high-resolution grids constructed by the National Geophysical Data Center or, in limited instances, internally. Each forecast model consists of three telescoped grids with increasing spatial and temporal resolution for simulation of wave inundation onto dry land. The forecast model utilizes the most recent bathymetry and topography available to reproduce the correct wave dynamics during the inundation computation. Forecast models are constructed for at-risk populous coastal communities in the Pacific and Atlantic Oceans. Previous and present development of forecast models in the Pacific (Titov *et al.*, 2005; Titov, 2009; Tang *et al.*, 2009; Wei *et al.*, 2008) have validated the accuracy and efficiency of the forecast models currently implemented in the SIFT system for real-time tsunami forecast. The model system is also a valuable tool in hind-cast research. Tang *et al.* (2009) provides forecast methodology details.

# 3.0 Model Development

Modeling of coastal communities is accomplished by development of a set of three nested grids that telescope down from a large spatial extent to a grid that finely defines the bathymetric and topographic features of the community under study. The original bathymetric and topographic grid data used in the development of the Arecibo model were provided by the National Geophysical Data Center (NGDC) under PMEL contract. Details of data gathering and grid construction techniques used by NGDC in the generation of the original grid are provided by Taylor *et al.* For each community, data are compiled from a variety of sources to produce a digital elevation model referenced to Mean High Water in the vertical and to the World Geodetic System 1984 in the horizontal (http://ngdc.noaa.gov/mgg/inundation/tsunami/inundation.html). From these digital elevation models, a set of three high-resolution reference models are constructed which are then "optimized" to run in an operationally specified period of time.

The bathymetry and topography used in the development of this forecast model was based on a digital elevation model provided by the National Geophysical Data Center and the author considers it to be an adequate representation of the local topography/bathymetry. As new digital elevation models become available, forecast models will be updated and report updates will be posted at <a href="http://nctr.pmel.noaa.gov/forecast\_reports/">http://nctr.pmel.noaa.gov/forecast\_reports/</a>.

# 3.1 Forecast Area

The city of Arecibo is nestled between the rivers Grande de Arecibo and Tanamá, on the northern coast of the island of Puerto Rico, approximately 70 km east of the capital city of San Juan. The population is estimated at 95,816 according the U.S. Census(2011). A medium size agricultural community, according to the Fundación Puertoriqueña de las Humanidades: "The fertility of the land in Arecibo favored the development of

agriculture, and the principal crop in the first half of the 20<sup>th</sup> century was sugar cane. Pineapple and other fruits were also planted. Arecibo also had a wealth of livestock ranches. The Arecibo River is known for its freshwater fish. Other sources of income for the municipality are the operation of various manufacturing factories in areas such as distilling and the production of paper, clothing, and chemical products." (Fundación Puertoriqueña de las Humanidades,

http://www.enciclopediapr.org/ing/article.cfm?ref=09022301&page=2).

Among the geographic features of Arecibo relevant to the evaluation of tsunami impact, are: The presence of a large coastal lagoon that extends for over 15 km to the East of Arecibo (see Figure 1), the valley carved by the Grande de Arecibo river, which defines the most likely inundation area, and the presence of several islets such as Punta Caracoles and Los Negritos which may pose some challenges to tsunami numerical simulations.

Puerto Rico is located at the northeastern corner of the Caribbean plates, on the boundary between the Caribbean and the North American plate. These two plates slide past each other in an oblique direction at a remarkably high rate of 2 cm/year for geological standards (USGS Science for a Changing World, Earthquake and Tsunamis in PR and the U.S. VI) as sketched in Figure 2. This generates a significant amount of seismicity north and south of the island. Clear evidence of this is that USGS research indicates equal probability for damaging ground motion for the town of Mayaguez in western Puerto Rico as for Seattle, WA (USGS Science for a Changing World, Earthquake and Tsunamis in PR and the U.S. VI). To the north of the island most of the tsunami-generating seismic events occur in the Puerto Rico Trench whereas the Muertos Trough is the generating area for tsunamis impacting the island from the south. Arecibo is located on the northern coast of the island of Puerto Rico, and it is, particularly vulnerable to tsunamis generated in the Puerto Rico Trench. However, far-field tsunamis originating in the Marqués de Pombal fault, offshore of Portugal have also been recorded on the island, such is the case of the 1755 Lisbon tsunami event. Table 1 contains a list of the most significant historical near-field seismic events in the island of Puerto Rico.

# 3.2 Historical Events and Data

A NOS (9757809) operated tide gauge was deployed on the Arecibo pier (18.48052° N, 66.70236° W) on March 5th 2007. The gauge is located by the breakwater on the northeastern corner of Arecibo Beach, extending southwest from the Arecibo lighthouse. The lower right panel of Figure 3 shows the location of the tide gauge within the inundation grid (grid C) of the forecast model. As mentioned earlier, Table 1 shows a list of the most significant recent near-field events impacting the island of Puerto Rico, however no tide gauge data of recent tsunamis at this location were found. So no tide gauge data could be used in the historical validation of this forecast model. Therefore the validation of the forecast model was based on comparison of high-resolution model results with forecast model results.

# 3.3 Model Setup

Setup of the computational grids for the Method of Splitting Tsunami code (MOST) (Titov, 1998) requires a total of 3 nested grids for which the outer grid A has the lowest spatial resolution, but covers the largest area, and the inner grid C has the highest spatial resolution, but covers a reduced geographical area. The code makes use of an additional intermediate grid B with medium resolution and spatial coverage. Each interior grid area is completely enclosed in the area covered by the next exterior grid, and inundation is computed only in the most interior grid (Grid C). The purpose of the set of three nested grids is to ensure that as the tsunami wavelength shrinks when it travels from deep to shallow waters, the model maintains an approximately constant number of grid nodes per wavelength. This set of 3 nested grids is forced by a pre-computed solution on an ocean wide grid at lower resolution (4 arc min x 4 arc min). The resolution of the this propagation grid was selected to mimic the effect of physical dispersion by manipulating numerical dispersion in the model (Burwell *et al.* 2007).

During the development of an operational forecast model, a higher resolution set of grids referred to as the reference model is generated first. The purpose of the reference model is to evaluate grid convergence between a high resolution model and the forecast model, ensuring that the solution obtained with the lower resolution forecast model is consistent with that computed with the high resolution reference model.

Several factors were determining in the design of the Arecibo model grids. One of them is the presence of extensive areas of extremely shallow water around the Caribbean arc. Tsunami waves propagating over these shallow regions will experience a shortening of their wavelength as they approach the island of Puerto Rico. It is important, therefore, to model wave propagation over these areas using a higher resolution grid than that used for the simulations stored in the deep-water propagation database (4 arc min resolution). This is accomplished in the present model by extending the most outer grid of the set of three nested grids (Grid A) towards the east and south of Puerto Rico. The resolution of Grid A in the present model is 47.24 arc sec in the zonal direction and 4 arc sec in the meridional direction, permitting the resolution of much higher frequency waves over shallow regions than the 4 arc min propagation database grid.

In addition, the A-grid used in the current forecast model is identical to that used in other Caribbean region forecast models, such as that for Charlotte Amalie in the U.S. Virgin Islands. This set up has the potential to be advantageous in future configurations of SIFT software, since it will make it possible to compute the A-grid only once and share the computation results with all forecast models located within the geographical extent of the grid, avoiding multiple computations of the same grid for different forecast models.

An additional consideration when designing the Arecibo forecast model grids was the local topography. The area around the town of Arecibo shows some regions of low-lying coastal planes susceptible of being inundated by tsunami waves. The southern boundary of the model's inundation grid (Grid C) was located far enough inland that most of the coastal plane is included in the grid. This configuration will ensure that even in the worst case scenario, tsunami runup will not exceed the grid boundaries.

The location of a densely populated coastal area mostly to the west of the tide gauge location was also a consideration when determining the location of the western boundary of the grid.

Figure 3 highlights the difference between the reference and the forecast model grids and Figures 4 and 5 show grid coverage area and relative grid position with respect to the community and local bathymetric features, for the reference and forecast models respectively. Table 2 summarizes the parameters and model set up for each set of grids.

### 4.0 Results and Discussion

Typically three types of tests are performed to assess the forecast model convergence, accuracy and robustness characteristics. However, in the case of Arecibo, since no historical data are available, accuracy tests based on historical events could not be performed.

To assess model convergence, results obtained with the reference model were compared with those obtained with the forecast model to confirm consistency of results at least for the leading tsunami waves. This type of test is not, strictly speaking, a grid convergence test in the sense used in computational science, since the solution is compared on grids with varying resolution, coverage and bathymetric information; however, it provides a good estimate of the similarities and discrepancies between the solution of a more accurate, high resolution model of the area and that of a coarser resolution run-time optimized forecast model.

Robustness tests include the simulation of 6 tsunamis generated by Mw 9.3 earthquakes throughout the Caribbean and Atlantic basin, a medium magnitude event (Mw=7.5) and a small magnitude (micro tsunami, Mw=6.2) event. Figure 6 shows the epicenter locations of these artificial events. Forecast model simulations proved to be free of instabilities during 24 hours of simulation for each of these synthetic mega events.

During the development of the present forecast model, it was observed when examining the animations of events with local co-seismic deformation in Arecibo, the presence of a west-travelling wave from the eastern boundary of the coastal lagoon (right edge of grid C) into the lagoon. The cause of this is that the current operational version of MOST modifies the local bathymetry in the case of local seismic deformation, but it does not modify the topography. Grid nodes interior to the coastal lagoon are considered bathymetric nodes (wet points) and experience subsidence during a local event. MOST applies the computed subsidence to these grid nodes, effectively lowering the water level in the lagoon below sea level. On the eastern boundary of the coastal lagoon (eastern edge of Grid C) wave values are interpolated from near-by exterior nodes in Grid B, some of those nodal values correspond to land values with 0 wave elevation. consequently the wave value along the eastern boundary of the lagoon is the average of some neighboring wet points (lagoon wet points in Grid B) and some dry points that fall outside of the lagoon in Grid B, the wet points have subsided below sea level due to the seismic deformation by the same amount as the lagoon wet points in Grid C, but the dry points maintain a wave height value of 0, resulting in a negative average interpolated wave height value to be interpolated into the lagoon boundary. The difference in wave height causes a positive wave to be interpolated into the eastern boundary of the lagoon. The problem was resolved by modifying the MOST code so that no bathymetric coseismic deformation was applied to the coastal lagoon, however this was a specific fix that worked for the Arecibo forecast model. When the forecast model is executed in SIFT it will run with the operational version of MOST and this left travelling wave will be visible in the lagoon for near-field simulations. This wave was small enough that it did not seem to have a major effect on the overall prediction.

#### 4.1 Model Validation

As there are no recorded historical cases for Arecibo, the validity of the forecast model was therefore assessed by comparing the forecast model solution with that obtained using the high resolution model for 8 synthetic scenarios. Since most of the tested scenarios are Mw=9.3, this set of tests was also used to establish the stability of the forecast model.

# 4.2 Model Stability Testing using Synthetic Scenarios

During model stability testing, 8 synthetic tsunamis (earthquake Mw 9.3, Mw 7.5, and Mw 6.2) were simulated using the forecast model. Details of the 8 synthetic events tested can be found in Table 3. Each of the six extreme synthetic mega events is constructed along a 1000 km long and 100 km wide fault plane with uniform slip amount of 25 m along the fault. The output from the code at every time step was visualized and inspected for instabilities. The cause of any instability was corrected and a final set of forecast grids emerged from the process. Most of the forecast model instabilities were associated with deficient resolution to distinguish small bathymetric and topographic features.

Six of the eight synthetic events used as test cases in this study were generated by earthquakes with epicenters located at different points along the Caribbean arc. The micro tsunami event (Mw=6.2) was designed to be generated by a far-field earthquake in the South Sandwich Islands. Time series comparison of the results obtained with the high resolution model and with the forecast model show very good agreement, with almost a one to one comparison during the first hour of simulation for all cases as evidenced in Figures 7 through 14. However, any differences between the high resolution and forecast model simulations during the first hour of simulation were reflected in discrepancies in the maximum amplitude of the wave train between both simulations. Some of the simulations such as those for Synthetic Scenarios 4 and 6 show excellent comparison between the two models even 24 hours into the simulation.

Of all six mega tsunami events tested, Synthetic Scenario 2 is the one posing the largest tsunami hazard to Arecibo with predicted wave amplitude of almost 15 m at the Arecibo tide gauge. Not surprisingly, Synthetic Scenario 2 represents a Mw=9.3 tsunami scenario generated in the Puerto Rico Trench, directly offshore of the coast of Arecibo. This is without a doubt the worst case scenario for Arecibo of all cases tested during the present study as evidenced in Figures D1 and D2 in Appendix D. Synthetic Scenario 2 is also the worst case scenario for the eastern seaboard of the United States. However, this scenario was designed merely to test the stability and performance of the forecast model during a very large local event. The credibility of such a scenario as a viable earthquake event at

that location has not been taken into consideration, consequently these results should not be interpreted as a tsunami hazard study for the Arecibo or the East coast of the United States, but as numerical exercises to test the computational stability of the forecast model. Additional cases generating a certain amount of inundation at Arecibo are Synthetic Scenarios 1 and 5, with tsunamis originating along the eastern segment of the Caribbean arc and off of the Caribbean coastline of Honduras, respectively. Figures 15 through 22 show the comparison between the inundation extents and maximum wave amplitudes for all 8 synthetic scenarios computed with the reference and forecast models.

# 5.0 Summary and Conclusion

A set of tsunami forecast grids has been developed for operational use by the Tsunami Warning Centers in conjunction with the Method of Splitting Tsunami code. Two sets of grids were developed: a high resolution set intended to provide reference values, and a forecast set designed to minimize processor run time and to provide real time tsunami estimates in Arecibo, Puerto Rico.

During model development, some geographical features unique to Arecibo such as the presence of very extensive shallow areas along the Caribbean arc and the presence of a coastal lagoon in the town of Arecibo were taken into consideration during the grid design process, some of these considerations will also affect the efficiency of future versions of the SIFT software, such as the ability to run a single Grid A for all locations in the island of Puerto Rico and the U.S. Virgin Islands.

The standard procedure, followed in the development of other forecast models in the Pacific Ocean, of testing the accuracy of the model with data from historical events and evaluating computed results with observations could not be performed in this case due to the lack of good quantitative data for recent historical tsunami events in the area. Therefore accuracy of the forecast model had to be evaluated in conjunction with its stability by comparing forecasted results of a series of mega-tsunami events with results obtained on a set of higher resolution grids.

Even though the magnitude of the set of synthetic events selected to perform stability tests on the forecast model may not necessarily represent credible seismic scenarios, the directivity of their tsunamis can be interpreted as an indicator of what parts of the Caribbean pose the largest tsunami hazard for Arecibo. In this respect, the results of our simulations show that an event in the Puerto Rico Trench immediately offshore of Arecibo represents the worst case scenario, followed by events from the East and West boundaries of the Caribbean arc.

The design of the forecast model grids to include the shallow water areas along the Caribbean arc with as high resolution as possible and the decision to share Grid A with the forecast model for Charlotte-Amalie, U.S. Virgin Islands had minor impact on processor run time and the forecast model was still capable of simulating 4 hours of tsunami activity in 11.35 minutes of wall clock time on an Intel Xeon E5670 2.3 processor.

# 6.0 Acknowledgments

This research is funded by the NOAA Center for Tsunami Research (NCTR). The authors would like to thank the modeling group of NCTR for their helpful suggestions and discussions. This publication is partially funded by the Joint Institute for the Study of the Atmosphere and Ocean (JISAO) under NOAA cooperative agreement No. NA17RJ1232, JISAO Contribution No. This is PMEL contribution No.

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http://factfinder2.census.gov/faces/tableservices/jsf/pages/productview.xhtml?pid=DEC\_ 10 DP DPDP1

USGS Science for a Changing World, Earthquake and Tsunamis in PR and the U.S. VI

http://maps.google.com/

# Appendix A

#### A1. Reference Model \*.in file for Arecibo

```
0.0001 Minimum amplitude of input offshore wave (m):
       Input minimum depth for offshore (m)
1
0.1
       Input "dry land" depth for inundation (m)
0.0009 Input friction coefficient (n**2)
1
       let a and b run up
300.0
       max eta before blow up (m)
.38
       Input time step (sec)
114000 Input amount of steps
5
       Compute "A" arrays every n-th time step, n=6
2
       Compute "B" arrays every n-th time step, n=
       Input number of steps between snapshots
80
       ...Starting from
1
       ...Saving grid every n-th node, n=
bathy/Anew20s 1nd SSL1.9sm.asc1
bathy/GridB RIM.crr.ssl
bathy/GridC RIM.crr.ssl.flt.snk3
../SRCS/Arecibo srcs/
./rsyn01 run2d/
1111
1
3 333 155
```

# A2. Forecast Model \*.in file for Arecibo

```
0.0001 Minimum amplitude of input offshore wave (m):
1
       Input minimum depth for offshore (m)
0.1
       Input "dry land" depth for inundation (m)
0.0009 Input friction coefficient (n**2)
1
       let a and b run up
300.0 max eta before blow up (m)
0.7
       Input time step (sec)
41300 Input amount of steps
       Compute "A" arrays every n-th time step, n=6
6
       Compute "B" arrays every n-th time step, n=
2
84
       Input number of steps between snapshots
```

```
    ...Starting from
    ...Saving grid every n-th node, n=
    arecibo_run2d/A5_45s_1nd_SSL1.9.asc
    arecibo_run2d/GridB_SIM.crr.ssl2
    arecibo_run2d/GridC_SIM.crr.ssl.flt.snk.ssl.9.crp2
    ./
    1 1 1 1 NetCDF output for A, B, C, SIFT
    Timeseries locations:
    3 118 78
```

# Appendix B

Propagation source details reflect the database as of January 2012. There may have been updates in the earthquake source parameters after this date

Earthquake location	Date	Magnitude		
Hispaniola	1953	6.9		
Mona Canyon	1946	7.5		
Hispaniola	1946	8.1		
Mona Canyon	1918	7.5		
Anegada Trough	1867	7.5		
Puerto Rico Trench	1787	8.1		

Model Setup	Reference Model			Forecast Model			
	Grid A	Grid B	Grid C	Grid A	Grid B	Grid C	
W	W69.90	W66.92	W66.80	W69.00	W66.87	W66.775	
Е	W60.50	W66.34	W66.63	W61.00	W66.53	W66.281	
S	N18.95	N18.70	N18.52	N18.95	N18.60	N18.522	
N	N16.05	N18.28	N18.41	N16.50	N18.35	N18.411	
dx	20.97"	6"	1"	47.24"	6"	2″	
dy	20"	6"	1"	45"	6"	2"	
nx × ny	1614×523	351x251	601×401	610×197	201x153	252×201	
dt (sec)	2.3	1.23	1.00	5.2	1.58	0.78	
D <sub>min</sub>	1 m			1 m			
Fric. (n <sup>2</sup> )	0.0009			0.0009			
CPU Time	~ 114.76 min for 4-hour simulation			~ 11.35 min for 4-hour simulation			
Warning Pt.	W66.70144, N18.47912						

SceNo.	Scenario Name	Source Zone	Tsunami Source	α (m)	Max (m)	Min (m)			
Mega-tsunami scenario									
1	ATSZ 38-47	Atlantic	A38-A47, A38-A47	25	2.52	-3.38			
2	ATSZ 48-57	Atlantic	A48-A57, B48-B57	25	14.3	-5.83			
3	ATSZ 58-67	Atlantic	A58-A67, B58-B67	25	0.52	-0.59			
4	ATSZ 68-77	Atlantic	A68-A77, B68-B77	25	0.11	-0.09			
5	ATSZ 82-91	Atlantic	A82-A91, B82-B91	25	3.17	-3.29			
6	SSSZ 1-10	South Sandwich	A1-A10, B1-B10	25	0.14	-0.14			
Mw 7.5 Tsunami scenario									
7	ATSZ B52	Atlantic	B52	1	0.10	-0.16			
Micro-tsunami scenario (select one)									
8	SSSZ B11	South Sandwich	B11	0.01	0.0002	-0.0003			

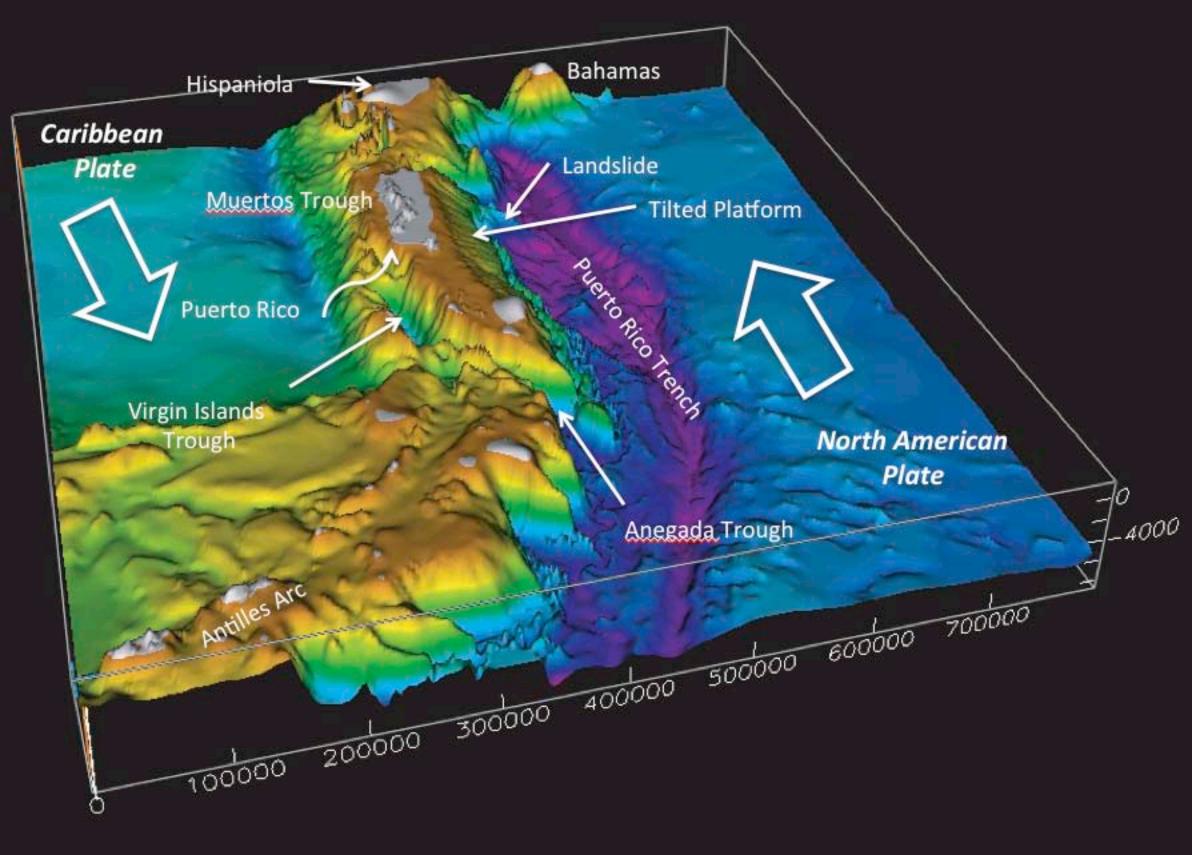
- **Figure 1**: Aerial view of the Puerto Arecibo showing the beach, the pier and location of the tide gauge to the right of the image, the mouth of the Grade de Arecibo River and population center to the left of the image (Google Maps).
- **Figure 2:** Schematic of tectonic motion and location of major bathymetric features in the neighborhood of Puerto Rico (from USGS Science for a Changing World, Earthquake and Tsunamis in PR and the U.S. VI).
- **Figure 3:** Comparison between the Reference and Forecast model grids. The location of the Arecibo tide gauge on the south side of the pier is indicated in the lower right panel.
- **Figure 4:** Map of the Northeastern Caribbean arc showing the relative position of the reference model grids relative to Arecibo and the island of Puerto Rico.
- **Figure 5:** Map of the Northeastern Caribbean arc showing the relative position of the forecast model grids relative to Arecibo and the island of Puerto Rico.
- **Figure 6:** Location of the mid-rupture point of the 8 synthetic (Mw=9.3) events used in the model robustness tests, showing the relative position of Puerto Rico to the epicenter locations.
- **Figure 7:** Comparison at the Arecibo tide gauge of the forecast and reference models for Synthetic Scenario 1.
- **Figure 8:** Comparison at the Arecibo tide gauge of the forecast and reference models for Synthetic Scenario 2.
- **Figure 9:** Comparison at the Arecibo tide gauge of the forecast and reference models for Synthetic Scenario 3.
- **Figure 10:** Comparison at the Arecibo tide gauge of the forecast and reference models for Synthetic Scenario 4.
- **Figure 11:** Comparison at the Arecibo tide gauge of the forecast and reference models for Synthetic Scenario 5.
- **Figure 12:** Comparison at the Arecibo tide gauge of the forecast and reference models for Synthetic Scenario 6.
- **Figure 13:** Comparison at the Arecibo tide gauge of the forecast and reference models for Synthetic Scenario 7.
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- **Figure 15:** Maximum sea surface elevation computed with the reference (left) and forecast (right) models for Synthetic Scenario 1.
- **Figure 16:** Maximum sea surface elevation computed with the reference (left) and forecast (right) models for Synthetic Scenario 2.
- **Figure 17:** Maximum sea surface elevation computed with the reference (left) and forecast (right) models for Synthetic Scenario 3.
- **Figure 18:** Maximum sea surface elevation computed with the reference (left) and forecast (right) models for Synthetic Scenario 4.

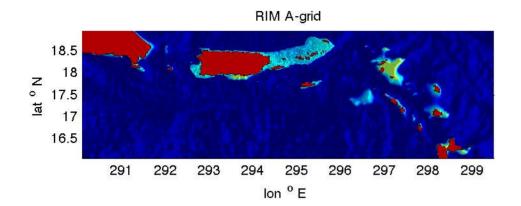
- **Figure 19:** Maximum sea surface elevation computed with the reference (left) and forecast (right) models for Synthetic Scenario 5.
- **Figure 20:** Maximum sea surface elevation computed with the reference (left) and forecast (right) models for Synthetic Scenario 6.
- **Figure 21:** Maximum sea surface elevation computed with the reference (left) and forecast (right) models for Synthetic Scenario 7.
- **Figure 22:** Maximum sea surface elevation computed with the reference (left) and forecast (right) models for Synthetic Scenario 8.
- **Figure C1:** Computed Atlantic-wide maximum sea surface elevation for Synthetic Scenarios 1-4.
- **Figure C2:** Computed Atlantic-wide maximum sea surface elevation for Synthetic Scenarios 5-8.

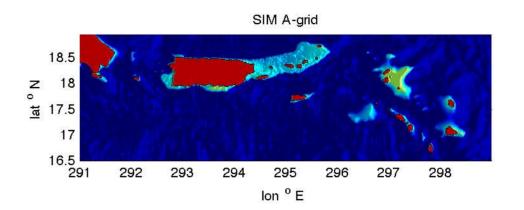
# List of Tables

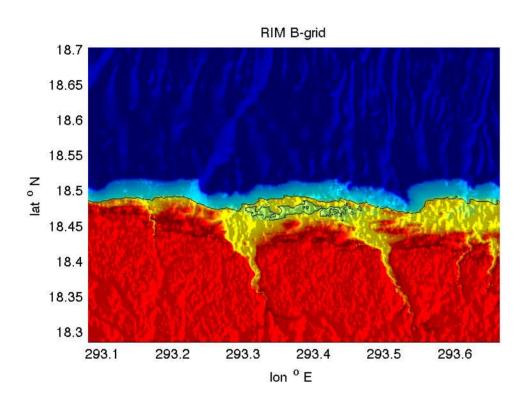
- 1 Most significant earthquakes in the Puerto Rico area in the last 3 centuries.
- 2 MOST setup parameters for reference and forecast models for Arecibo.
- 3 Synthetic tsunami sources used in the forecast model stability test for Arecibo showing tide gauge max and min water level elevations.

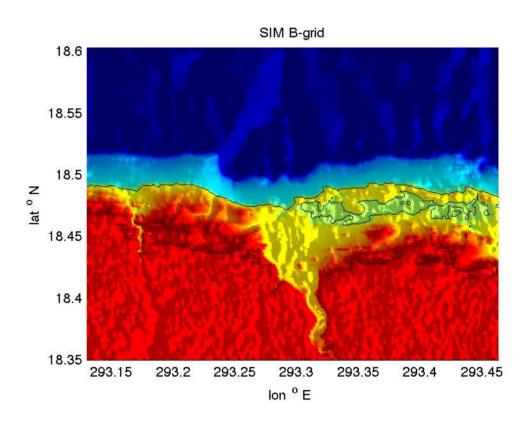


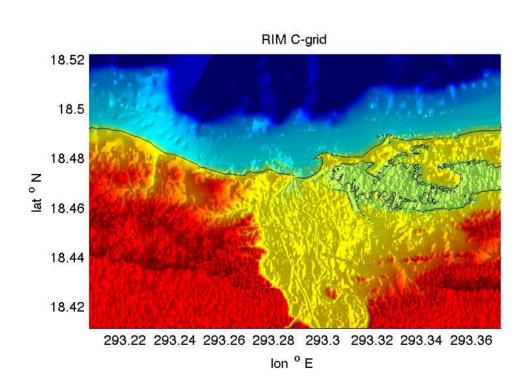


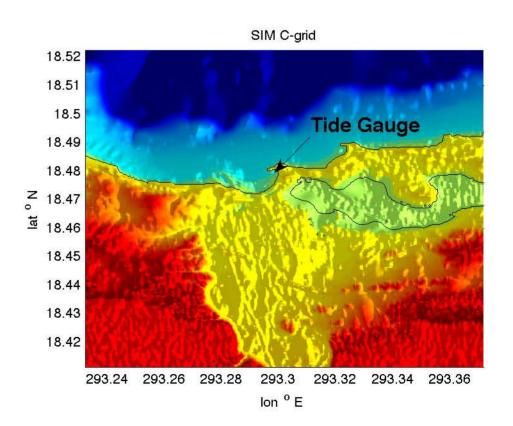


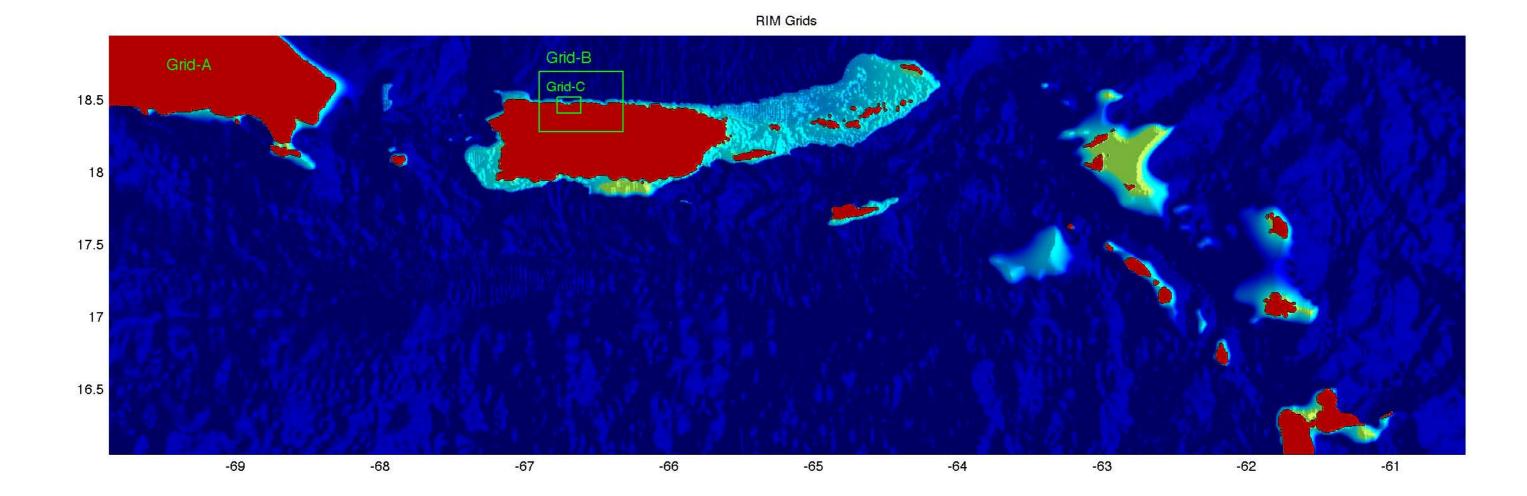


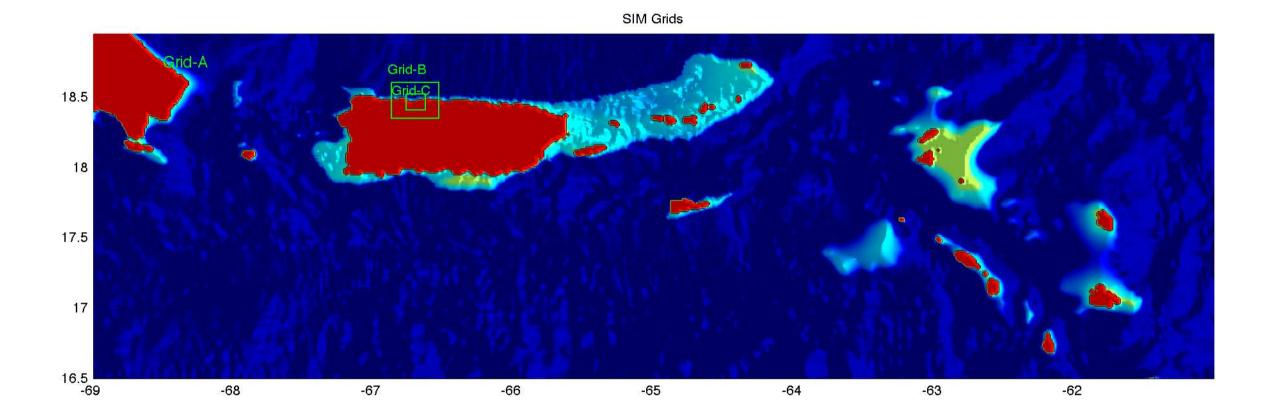


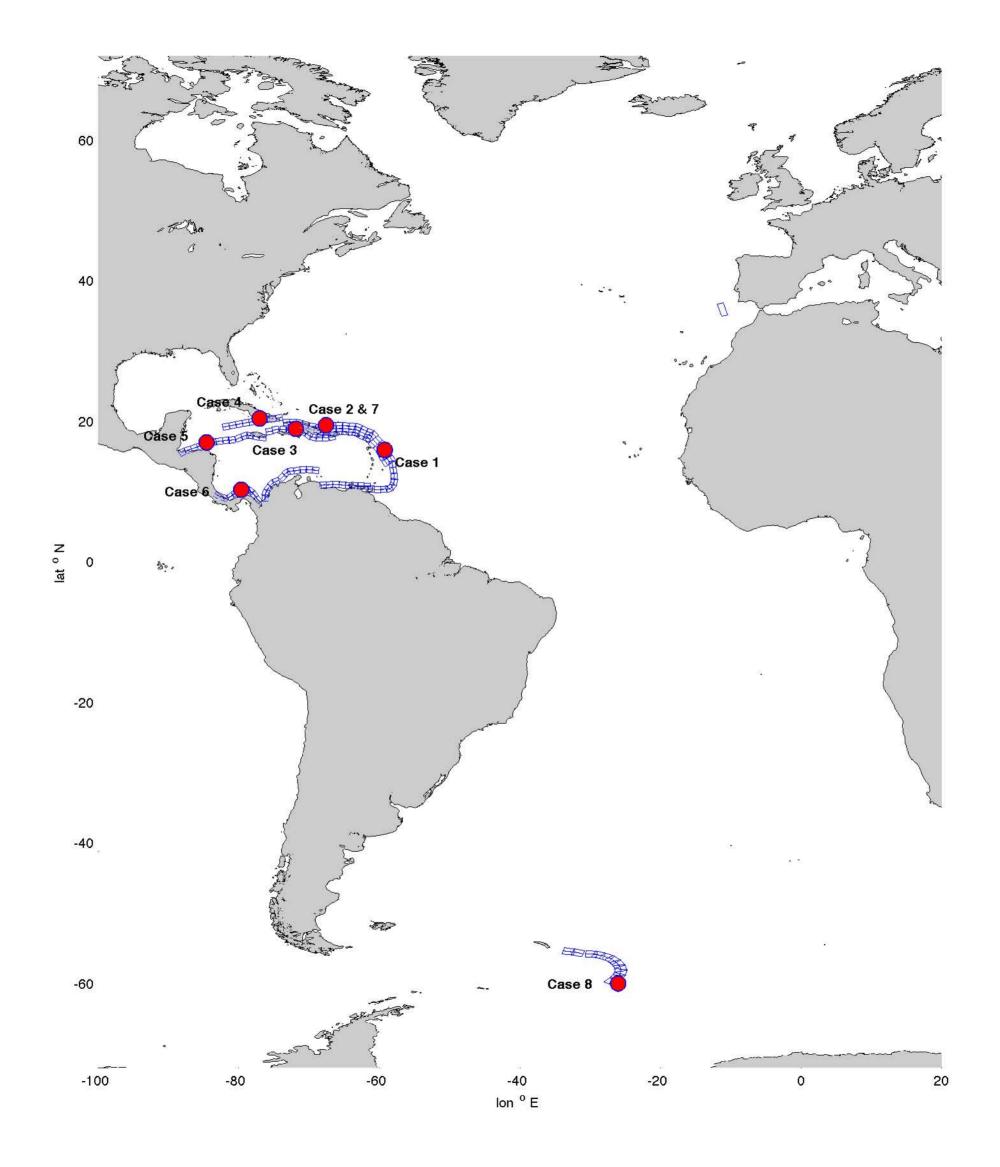


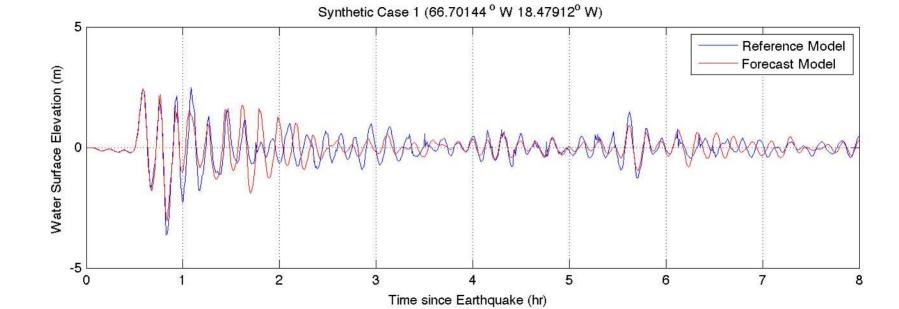


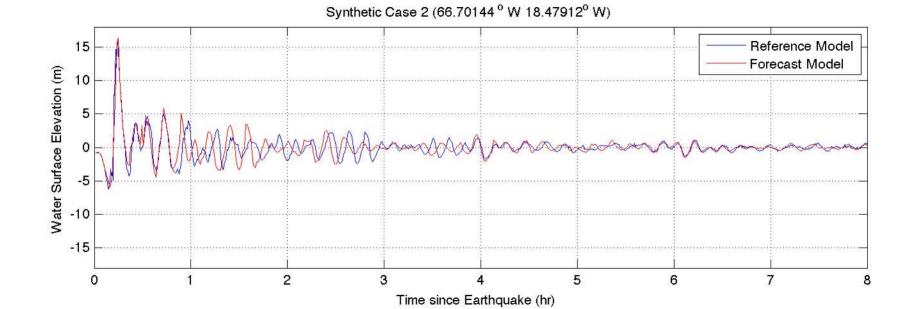


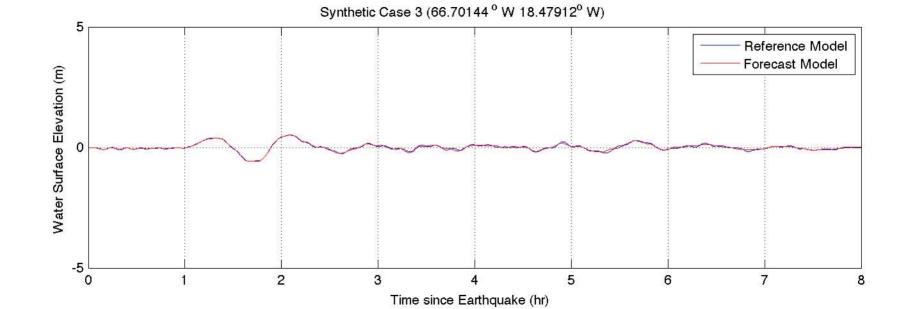


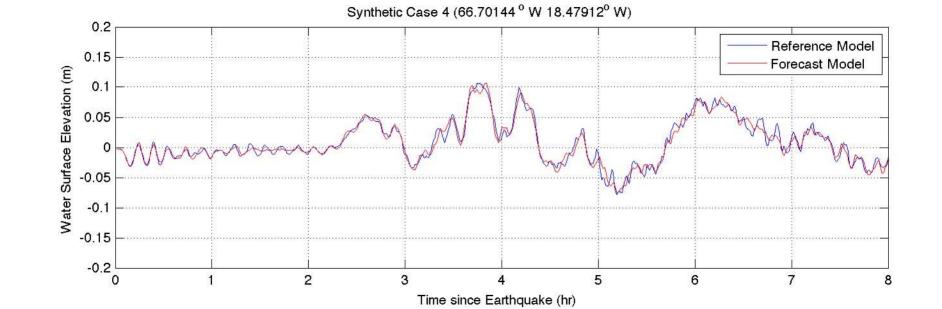


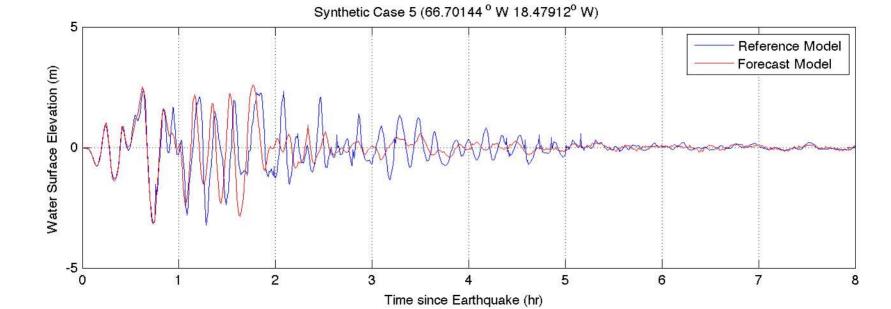


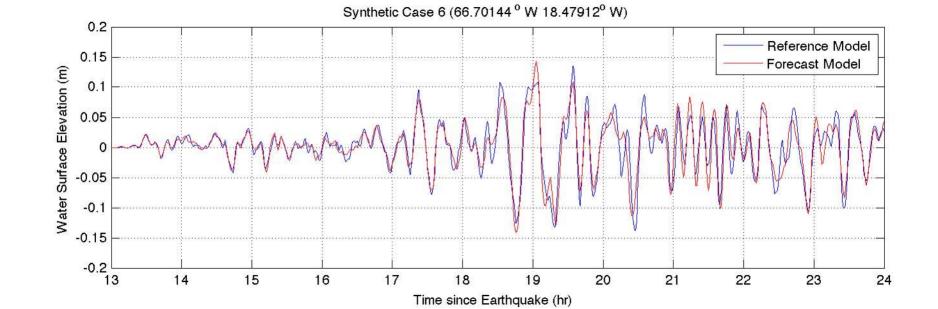


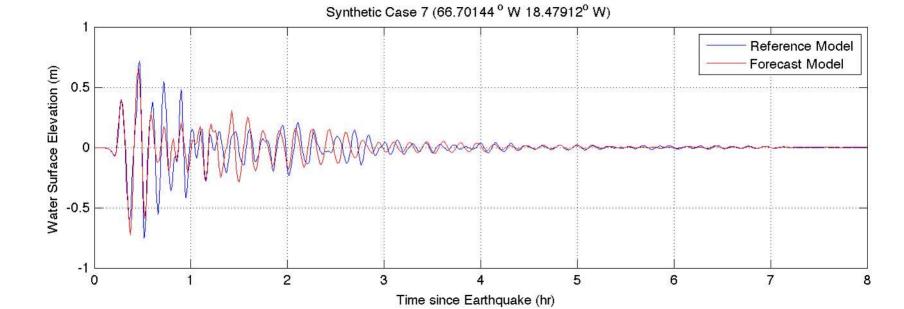


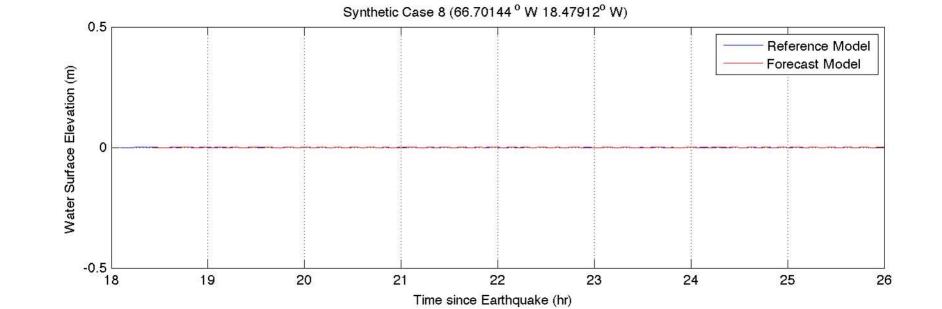


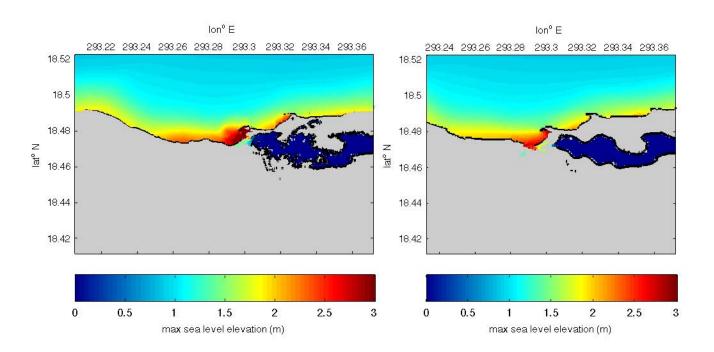


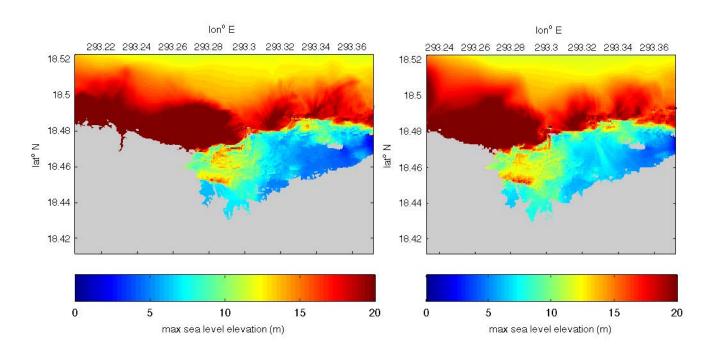


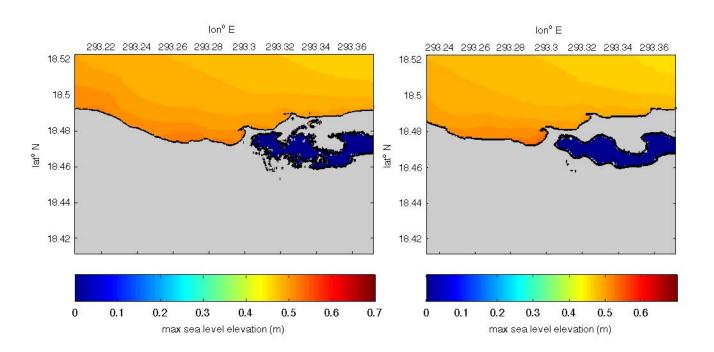


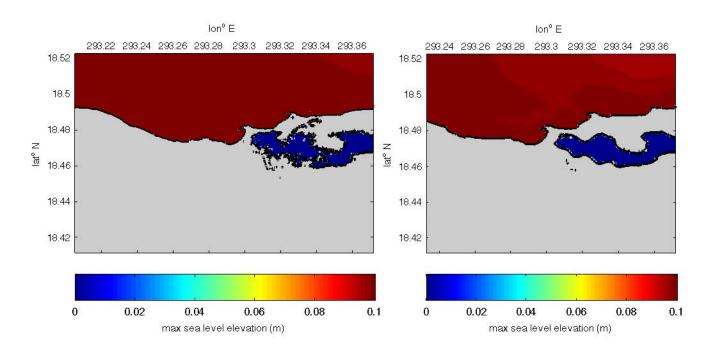


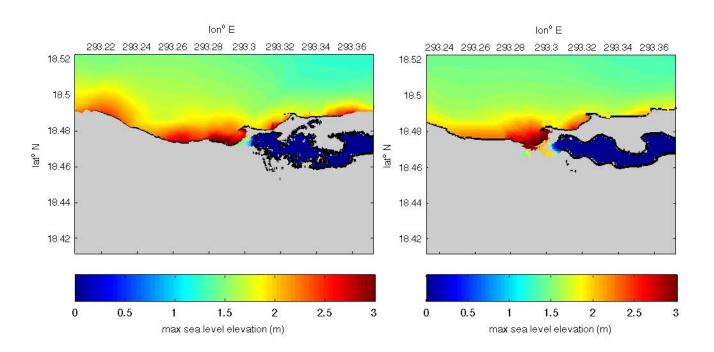


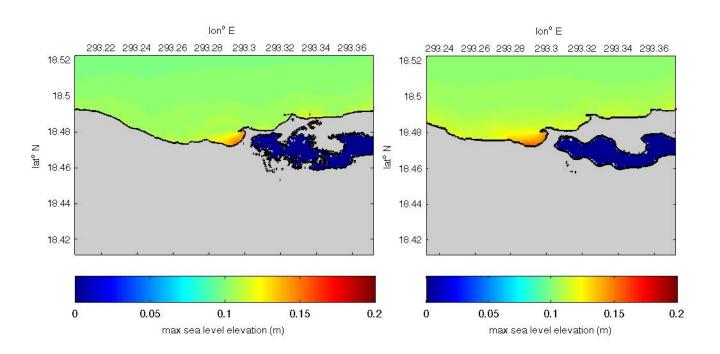


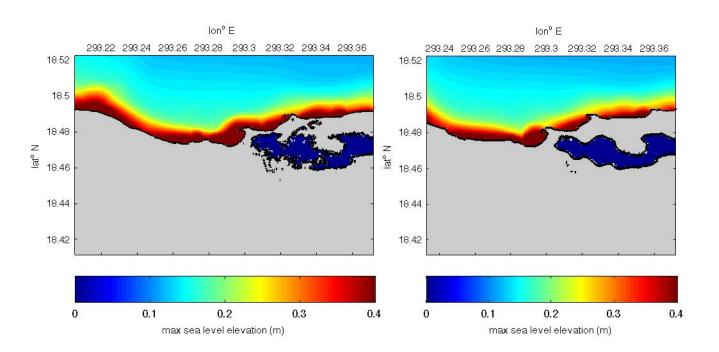


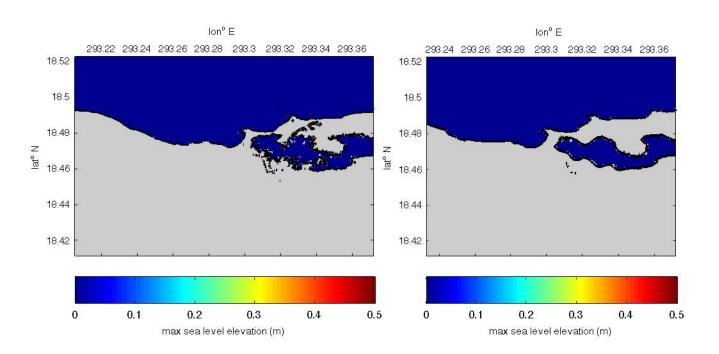












# Appendix B

## Propagation Database: Atlantic Ocean Unit Sources

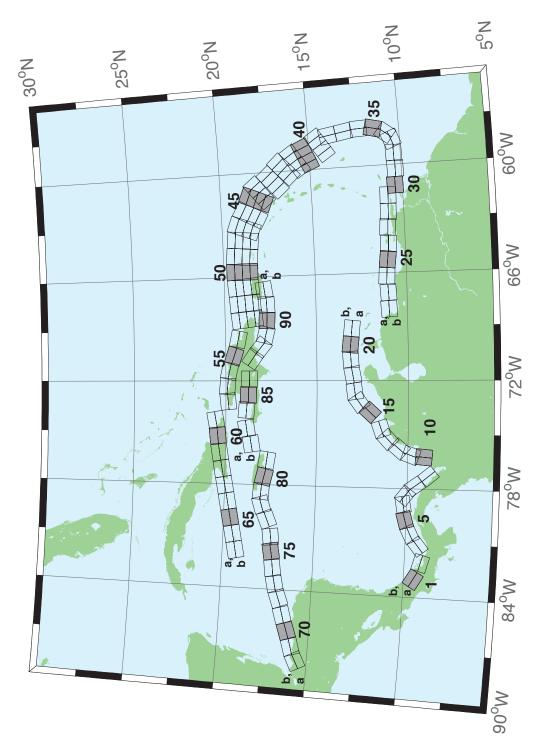


Figure B.1: Atlantic Source Zone unit sources.

Table B.1: Earthquake parameters for Atlantic Source Zone unit sources.

Segm	ent	Description	Lo	ngitude(°E)	Latitude(°N)	Strike(°)	Dip(°)	Depth (km)
atsz–1a	Atl	antic Source Z	Zone	-83.2020	9.1449	120	27.5	5 28.09
atsz-1b	Atl	antic Source Z	Zone	-83.0000	9.4899	120	27.5	5 5
atsz-2a	Atl	antic Source Z	Zone	-82.1932	8.7408	105.1	27.5	5   28.09
atsz-2b	Atl	antic Source Z	Zone	-82.0880	9.1254	105.1	. 27.5	5 5
atsz-3a	Atl	antic Source Z	Zone	-80.9172	9.0103	51.31	. 30	30
atsz-3b	Atl	antic Source Z	Zone	-81.1636	9.3139	51.31	. 30	5
atsz-4a	Atl	antic Source Z	Zone	-80.3265	9.4308	63.49	30	30
atsz-4b	Atl	antic Source Z	Zone	-80.5027	9.7789	63.49	30	5
atsz-5a	Atl	antic Source Z	Zone	-79.6247	9.6961	74.44	30	30
atsz-5b	Atl	antic Source Z	Zone	-79.7307	10.0708	74.44	30	5
atsz-6a	Atl	antic Source Z	Zone	-78.8069	9.8083	79.71	. 30	30
atsz-6b	Atl	antic Source Z	Zone	-78.8775	10.1910	79.71	. 30	5
atsz-7a	Atl	antic Source Z	Zone	-78.6237	9.7963	127.2	30	30
atsz-7b	Atl	antic Source Z	Zone	-78.3845	10.1059	127.2	30	5
atsz-8a	Atl	antic Source Z	Zone	-78.1693	9.3544	143.8	30	30
atsz-8b	Atl	antic Source Z	Zone	-77.8511	9.5844	143.8	30	5
atsz-9a	Atl	antic Source Z	Zone	-77.5913	8.5989	139.9	30	30
atsz-9b	Atl	antic Source Z	Zone	-77.2900	8.8493	139.9	30	5
atsz-10a	Atl	antic Source Z	Zone	-75.8109	9.0881	4.67	17	19.62
atsz-10b	Atl	antic Source Z	Zone	-76.2445	9.1231	4.67	17	5
atsz-11a	Atl	antic Source Z	Zone	-75.7406	9.6929	19.67	17	19.62
atsz-11b	Atl	antic Source Z	Zone	-76.1511	9.8375	19.67	17	5
atsz-12a	Atl	antic Source Z	Zone	-75.4763	10.2042	40.4	17	19.62
atsz-12b	Atl	antic Source Z	Zone	-75.8089	10.4826	40.4	17	5
atsz-13a	Atl	antic Source Z	Zone	-74.9914	10.7914	47.17	17	19.62
atsz-13b	Atl	antic Source Z	Zone	-75.2890	11.1064	47.17	17	5
atsz-14a	Atl	antic Source Z	Zone	-74.5666	11.0708	71.68	3 17	19.62
atsz-14b	Atl	antic Source Z	Zone	-74.7043	11.4786	71.68	3 17	5
atsz-15a	Atl	antic Source Z	Zone	-73.4576	11.8012	42.69	17	19.62
atsz-15b	Atl	antic Source Z	Zone	-73.7805	12.0924	42.69	17	5
atsz-16a	Atl	antic Source Z	Zone	-72.9788	12.3365	54.75	17	19.62
atsz-16b	Atl	antic Source Z	Zone	-73.2329	12.6873	54.75	17	5
atsz-17a	Atl	antic Source Z	Zone	-72.5454	12.5061	81.96	17	19.62
atsz-17b	Atl	antic Source Z	Zone	-72.6071	12.9314	81.96	17	5
atsz-18a	Atl	antic Source Z	Zone	-71.6045	12.6174	79.63	17	19.62
atsz-18b	Atl	antic Source Z	Zone	-71.6839	13.0399	79.63	17	5
atsz-19a	Atl	antic Source Z	Zone	-70.7970	12.7078	86.32	17	19.62
atsz-19b	Atl	antic Source Z	Zone	-70.8253	13.1364	86.32	2 17	5
atsz-20a	Atl	antic Source Z	Zone	-70.0246	12.7185	95.94	17	19.62
atsz-20b	Atl	antic Source Z	Zone	-69.9789	13.1457	95.94	17	5
atsz-21a	Atl	antic Source Z	Zone	-69.1244	12.6320	95.94	17	19.62
atsz-21b	Atl	antic Source Z	Zone	-69.0788	13.0592	95.94	17	5
atsz-22a	Atl	antic Source Z	Zone	-68.0338	11.4286	266.9		17.94
atsz-22b	Atl	antic Source Z	Zone	-68.0102	10.9954	266.9	15	5
atsz-23a	Atl	antic Source Z	Zone	-67.1246	11.4487	266.9	15	17.94
atsz $-23b$		antic Source Z		-67.1010	11.0155	266.9		5
atsz-24a		antic Source Z		-66.1656	11.5055	273.3		17.94
atsz $-24b$		antic Source Z		-66.1911	11.0724	273.3		5
atsz-25a		antic Source Z		-65.2126	11.4246	276.4		
atsz-25b		antic Source Z		-65.2616	10.9934	276.4		
atsz–26a		antic Source Z		-64.3641	11.3516	272.9		17.94
atsz–26b		antic Source Z		-64.3862	10.9183	272.9		
atsz–27a		antic Source Z		-63.4472	11.3516	272.9		17.94
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Table B.1 – continued from previous page

Table B.1 – continued from previous page								
_S	Segment	Description	Lor	ngitude(°E)	Latitude(°N)	Strike(°)	Dip(°)	Depth (km)
atsz-2		lantic Source		-63.4698	10.9183	272.9		
atsz-2	28a At	lantic Source	Zone	-62.6104	11.2831	271.1	. 15	17.94
atsz-2		lantic Source	Zone	-62.6189	10.8493	271.1	. 15	
atsz-2	29a At	lantic Source	Zone	-61.6826	11.2518	271.6	15	
atsz-2	29b At	lantic Source	Zone	-61.6947	10.8181	271.6	15	5
atsz-3	30a At	lantic Source	Zone	-61.1569	10.8303	269	15	17.94
atsz-3	30b At	lantic Source	Zone	-61.1493	10.3965	269	15	5
atsz-3	31a At	lantic Source	Zone	-60.2529	10.7739	269	15	17.94
atsz-3	31b At	lantic Source	Zone	-60.2453	10.3401	269	15	5
atsz-3	32a At	lantic Source	Zone	-59.3510	10.8123	269	15	17.94
atsz-3	32b At	lantic Source	Zone	-59.3734	10.3785	269	15	5
atsz-3	3a At	lantic Source	Zone	-58.7592	10.8785	248.6	15	17.94
atsz-3	3b At	lantic Source	Zone	-58.5984	10.4745	248.6	15	5
atsz-3	84a At	lantic Source	Zone	-58.5699	11.0330	217.2	2 15	17.94
atsz-3		lantic Source		-58.2179	10.7710	217.2	2 15	5
atsz-3		lantic Source		-58.3549	11.5300	193.7	15	17.94
atsz-3	35b At	lantic Source	Zone	-57.9248	11.4274	193.7		5
atsz-3		lantic Source		-58.3432	12.1858	177.7		
atsz-3		lantic Source		-57.8997	12.2036	177.7		
atsz-3		lantic Source		-58.4490	12.9725	170.7		
atsz-3		lantic Source		-58.0095	13.0424	170.7		
atsz-3		lantic Source		-58.6079	13.8503	170.2		
atsz-3		lantic Source		-58.1674	13.9240	170.2		
atsz-3		lantic Source		-58.6667	14.3915	146.8		
atsz-3		lantic Source		-58.2913	14.6287	146.8		
atsz-3		lantic Source		-59.4168	13.9171	146.8		
atsz-3	v	lantic Source		-59.0415	14.1543	146.8		
atsz-4		lantic Source		-59.1899	15.2143	156.2		
atsz-4		lantic Source		-58.7781	15.3892	156.2		
atsz-4		lantic Source		-60.0131	14.8646	156.2		
atsz-4		lantic Source		-59.6012	15.0395	156.2		
atsz-4		lantic Source		-59.4723	15.7987	146.3		
atsz-4		lantic Source		-59.0966	16.0392	146.3		
		lantic Source						
atsz-4	v	lantic Source		-60.2229	15.3177	146.3		
atsz-4 atsz-4				-59.8473	15.5582	146.3	15	
		lantic Source		-59.9029	16.4535	137		
atsz-4		lantic Source		-59.5716	16.7494	137	15	
atsz-4	v	lantic Source		-60.5645	15.8616	137	15	
atsz–4		lantic Source		-60.2334	16.1575	137	15	
atsz–4		lantic Source		-60.5996	17.0903	138.7		
atsz–4		lantic Source		-60.2580	17.3766	138.7		
atsz–4		lantic Source		-61.2818	16.5177	138.7		
atsz–4		lantic Source		-60.9404	16.8040	138.7		
atsz–4		lantic Source		-61.1559	17.8560	141.1		
atsz–4		lantic Source		-60.8008	18.1286	141.1		
atsz–4		lantic Source		-61.8651	17.3108	141.1		
atsz–4		lantic Source		-61.5102	17.5834	141.1		
atsz–4		lantic Source		-61.5491	18.0566	112.8		
atsz–4		lantic Source		-61.3716	18.4564	112.8		
atsz-4		lantic Source		-61.9037	17.2569	112.8	3 15	43.82
atsz-4		lantic Source		-61.7260	17.6567	112.8	3 15	
atsz-4	l6a At	lantic Source	Zone	-62.4217	18.4149	117.9	15	17.94
atsz-4	l6b At	lantic Source	Zone	-62.2075	18.7985	117.9	15	5
atsz-4	l6y At	lantic Source	Zone	-62.8493	17.6477	117.9	15	43.82
atsz-4	l6z At	lantic Source	Zone	-62.6352	18.0313	117.9		
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Table B.1 – continued from previous page

_		'	Table E	3.1 – conti	nued from prev	vious page		
_	Segmen	t Description	Long	itude(°E)	Latitude(°N)	Strike(°)	Dip(°)	Depth (km)
atsz		Atlantic Source		-63.1649	18.7844	110.5		
atsz-		Atlantic Source		-63.0087	19.1798	110.5		
atsz-		Atlantic Source		-63.4770	17.9936	110.5		
atsz	-47z	Atlantic Source	Zone	-63.3205	18.3890	110.5	20	39.2
atsz	–48a A	Atlantic Source	Zone	-63.8800	18.8870	95.37	20	22.1
atsz	-48b A	Atlantic Source	Zone	-63.8382	19.3072	95.37	20	
atsz-	-48y	Atlantic Source	Zone	-63.9643	18.0465	95.37	20	56.3
atsz-	-48z	Atlantic Source	Zone	-63.9216	18.4667	95.37	20	39.2
atsz-	-49a A	Atlantic Source	Zone	-64.8153	18.9650	94.34	20	22.1
atsz-	–49b <i>A</i>	Atlantic Source	Zone	-64.7814	19.3859	94.34	20	5
atsz-	–49y	Atlantic Source	Zone	-64.8840	18.1233	94.34	20	56.3
atsz-	-49z	Atlantic Source	Zone	-64.8492	18.5442	94.34	20	39.2
atsz-	-50a A	Atlantic Source	Zone	-65.6921	18.9848	89.59	20	22.1
atsz-	-50b	Atlantic Source	Zone	-65.6953	19.4069	89.59	20	5
atsz-	-50y	Atlantic Source	Zone	-65.6874	18.1407	89.59	20	56.3
atsz-	-50z	Atlantic Source	Zone	-65.6887	18.5628	89.59	20	39.2
atsz-	-51a A	Atlantic Source	Zone	-66.5742	18.9484	84.98	3 20	22.1
atsz-	-51b A	Atlantic Source	Zone	-66.6133	19.3688	84.98	3 20	5
		Atlantic Source		-66.4977	18.1076	84.98		
atsz-	·	Atlantic Source		-66.5353	18.5280	84.98	3 20	
		Atlantic Source		-67.5412	18.8738	85.87		
		Atlantic Source		-67.5734	19.2948	85.87		
atsz-		Atlantic Source	Zone	-67.4781	18.0319	85.87		
atsz-	·	Atlantic Source		-67.5090	18.4529	85.87		
		Atlantic Source		-68.4547	18.7853	83.64		
		Atlantic Source		-68.5042	19.2048	83.64		
atsz-		Atlantic Source		-68.3575	17.9463	83.64		
atsz-		Atlantic Source		-68.4055	18.3658	83.64		
		Atlantic Source		-69.6740	18.8841	101.5		
		Atlantic Source		-69.5846	19.2976	101.5		
		Atlantic Source		-70.7045	19.1376	108.2		
		Atlantic Source		-70.5647	19.5386	108.2		
atsz-		Atlantic Source		-71.5368	19.3853	100.2		
		Atlantic Source		-71.4386	19.7971	102.6		
		Atlantic Source		-72.3535	19.4838	94.2	20	
		Atlantic Source		-72.3206	19.9047	94.2	20	
		Atlantic Source		-73.1580		84.34		
		Atlantic Source			19.4498			
				-73.2022	19.8698	84.34		
		Atlantic Source Atlantic Source		-74.3567 -74.2764	20.9620	259.7 259.7		
					20.5467			
		Atlantic Source		-75.2386 75.1017	20.8622	264.2		
		Atlantic Source		-75.1917	20.4306	264.2		
		Atlantic Source		-76.2383	20.7425	260.7		
		Atlantic Source		-76.1635	20.3144	260.7		
		Atlantic Source		-77.2021	20.5910	259.9		
atsz-		Atlantic Source		-77.1214	20.1638	259.9		
		Atlantic Source		-78.1540	20.4189	259	15	
		Atlantic Source		-78.0661	19.9930	259	15	
		Atlantic Source		-79.0959	20.2498	259.2		
		Atlantic Source		-79.0098	19.8236	259.2		
		Atlantic Source		-80.0393	20.0773	258.9		
		Atlantic Source		-79.9502	19.6516	258.9		
		Atlantic Source		-80.9675	19.8993	258.6		
		Atlantic Source		-80.8766	19.4740	258.6		5
atsz-	–67a <i>A</i>	Atlantic Source	Zone	-81.9065	19.7214	258.5		
						C	ontinued of	on next page

Table B.1 - continued from previous page

-	Commont	Description	Los		Latituda(ON)		Din(0)	Donth (lrm)
_	Segment	Description	LOI	ngitude(°E)	Latitude(°N)	Strike(°)	Dip(°)	Depth (km)
atsz		tlantic Source		-81.8149	19.2962	258.5	-	5
atsz-	-68a A	tlantic Source	Zone	-87.8003	15.2509	62.69	15	17.94
atsz-		tlantic Source		-88.0070	15.6364	62.69	_	5
atsz-	-69a A	tlantic Source	Zone	-87.0824	15.5331	72.73	15	17.94
atsz-	-69b A	tlantic Source	Zone	-87.2163	15.9474	72.73	15	5
atsz		tlantic Source		-86.1622	15.8274	70.64	-	17.94
atsz	-70b A	tlantic Source	Zone	-86.3120	16.2367	70.64	15	5
atsz-	-71a A	tlantic Source	Zone	-85.3117	16.1052	73.7	15	17.94
atsz	-71b A	tlantic Source	Zone	-85.4387	16.5216	73.7	15	5
atsz-		tlantic Source		-84.3470	16.3820	69.66	15	17.94
atsz-	-72b A	tlantic Source	Zone	-84.5045	16.7888	69.66	15	5
atsz-	-73a A	tlantic Source	Zone	-83.5657	16.6196	77.36		17.94
atsz-		tlantic Source		-83.6650	17.0429	77.36		5
atsz-		tlantic Source		-82.7104	16.7695	82.35		17.94
atsz		tlantic Source		-82.7709	17.1995	82.35		5
atsz-		tlantic Source		-81.7297	16.9003	79.86	_	17.94
atsz		tlantic Source		-81.8097	17.3274	79.86		5
atsz		tlantic Source		-80.9196	16.9495	82.95		17.94
atsz		tlantic Source		-80.9754	17.3801	82.95		5
atsz		tlantic Source		-79.8086	17.2357	67.95	_	17.94
atsz		tlantic Source		-79.9795	17.6378	67.95		5
atsz-		tlantic Source		-79.0245	17.5415	73.61		17.94
atsz-		tlantic Source		-79.1532	17.9577	73.61		5
atsz-		tlantic Source		-78.4122	17.5689	94.07		17.94
atsz-		tlantic Source		-78.3798	18.0017	94.07	_	5
atsz-		tlantic Source		-77.6403	17.4391	103.3		17.94
atsz-		tlantic Source		-77.5352	17.8613	103.3	_	5
atsz-		tlantic Source		-76.6376	17.2984	98.21		17.94
atsz-	-	tlantic Source		-76.5726	17.7278	98.21	_	5
atsz-		tlantic Source		-75.7299	19.0217	260.1		17.94
atsz-	-	tlantic Source		-75.6516	18.5942	260.1		5
atsz-		tlantic Source		-74.8351	19.2911	260.8		17.94
atsz-		tlantic Source		-74.7621	18.8628	260.8		5
atsz-		tlantic Source		-73.6639	19.2991	274.8	_	17.94
atsz-		tlantic Source tlantic Source		-73.7026 -72.8198	18.8668 19.2019	274.8 $270.6$		$\frac{5}{17.94}$
atsz-		tlantic Source		-72.8246	18.7681	270.6	_	17.94
atsz-		tlantic Source		-72.8240 -71.9143	19.1477	269.1	_	17.94
atsz-		tlantic Source		-71.9145 -71.9068	18.7139	269.1	_	17.94
atsz-		tlantic Source		-70.4738	18.8821	304.5	_	17.94
atsz-		tlantic Source		-70.7329	18.5245	304.5	_	5
atsz-		tlantic Source		-69.7710	18.3902	304.5	_	17.94
atsz-		tlantic Source		-70.0547	18.0504	308.4	_	17.94
atsz-		tlantic Source		-69.2635	18.2099	283.9	_	17.94
atsz-		tlantic Source		-69.3728	17.7887	283.9 283.9		17.94
atsz		tlantic Source		-68.5059	18.1443	272.9		17.94
atsz-		tlantic Source		-68.5284	17.7110	272.9	_	5
atsz-		tlantic Source		-67.6428	18.1438	267.8	_	17.94
atsz		tlantic Source		-67.6256	17.7103	267.8	_	5
atsz-	-	tlantic Source		-66.8261	18.2536	262	15	17.94
atsz-		tlantic Source		-66.7627	17.8240	262	15	5
	11			50521	11.0210			

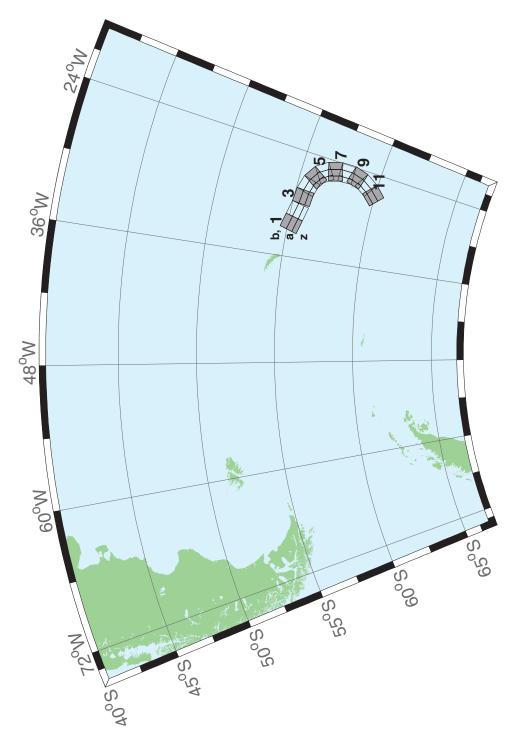


Figure B.2: South Sandwich Islands Subduction Zone.

 ${\bf Table~B.2:~Earthquake~parameters~for~South~Sandwich~Islands~Subduction~Zone~unit~sources.}$ 

•	Segment Description	Longitude(°E)	Latitude(°N)	Strike(°) Dip(°)	Depth (km	)	
sssz–1a	South Sandwich Isla	nds Subduction Zon	e -32.3713	-55.4655	104.7	28.53	17.51
sssz-1b	South Sandwich Isla	nds Subduction Zon	e -32.1953	-55.0832	104.7	9.957	8.866
sssz-1z	South Sandwich Isla	nds Subduction Zon	e -32.5091	-55.7624	104.7	46.99	41.39
sssz-2a	South Sandwich Isla	nds Subduction Zon	e -30.8028	-55.6842	102.4	28.53	17.51
sssz-2b	South Sandwich Isla	nds Subduction Zon	e -30.6524	-55.2982	102.4	9.957	8.866
sssz-2z	South Sandwich Isla	nds Subduction Zon	e -30.9206	-55.9839	102.4	46.99	41.39
sssz-3a	South Sandwich Isla	nds Subduction Zon	e -29.0824	-55.8403	95.53	28.53	17.51
sssz-3b	South Sandwich Isla	nds Subduction Zon	e -29.0149	-55.4468	95.53	9.957	8.866
sssz-3z	South Sandwich Isla	nds Subduction Zon	e -29.1353	-56.1458	95.53	46.99	41.39
sssz-4a	South Sandwich Isla	nds Subduction Zon	e -27.8128	-55.9796	106.1	28.53	17.51
sssz-4b	South Sandwich Isla	nds Subduction Zon	e -27.6174	-55.5999	106.1	9.957	8.866
sssz-4z	South Sandwich Isla	nds Subduction Zon	e -27.9659	-56.2744	106.1	46.99	41.39
sssz-5a	South Sandwich Isla	nds Subduction Zon	e -26.7928	-56.2481	123.1	28.53	17.51
sssz-5b	South Sandwich Isla	nds Subduction Zon	e -26.4059	-55.9170	123.1	9.957	8.866
sssz-5z	South Sandwich Isla	nds Subduction Zon	e -27.0955	-56.5052	123.1	46.99	41.39
sssz-6a	South Sandwich Isla	nds Subduction Zon	e -26.1317	-56.6466	145.6	23.28	16.11
sssz-6b	South Sandwich Isla	nds Subduction Zon	e -25.5131	-56.4133	145.6	9.09	8.228
sssz-6z	South Sandwich Isla	nds Subduction Zon	e -26.5920	-56.8194	145.6	47.15	35.87
sssz-7a	South Sandwich Isla	nds Subduction Zon	e -25.6787	-57.2162	162.9	21.21	14.23
sssz-7b	South Sandwich Isla	nds Subduction Zon	e -24.9394	-57.0932	162.9	7.596	7.626
sssz-7z	South Sandwich Isla	nds Subduction Zon	e -26.2493	-57.3109	162.9	44.16	32.32
sssz-8a	South Sandwich Isla	nds Subduction Zon	e -25.5161	-57.8712	178.2	20.33	15.91
sssz-8b	South Sandwich Isla	nds Subduction Zon	e -24.7233	-57.8580	178.2	8.449	8.562
sssz-8z	South Sandwich Isla	nds Subduction Zon	e -26.1280	-57.8813	178.2	43.65	33.28
sssz-9a	South Sandwich Isla	nds Subduction Zon	e -25.6657	-58.5053	195.4	25.76	15.71
sssz-9b	South Sandwich Isla	nds Subduction Zon	e -24.9168	-58.6127	195.4	8.254	8.537
sssz-9z	South Sandwich Isla	nds Subduction Zon	e -26.1799	-58.4313	195.4	51.69	37.44
sssz-10a	a South Sandwich Isla	nds Subduction Zon	e -26.1563	-59.1048	212.5	32.82	15.65
sssz-10b	South Sandwich Isla	nds Subduction Zon	e -25.5335	-59.3080	212.5	10.45	6.581
sssz-10z	South Sandwich Isla	nds Subduction Zon	e -26.5817	-58.9653	212.5	54.77	42.75
sssz–11a	a South Sandwich Isla	nds Subduction Zon	e -27.0794	-59.6799	224.2	33.67	15.75
sssz-11b	South Sandwich Isla	nds Subduction Zon	e -26.5460	-59.9412	224.2	11.32	5.927
sssz-11z	South Sandwich Isla	nds Subduction Zon	e -27.4245	-59.5098	224.2	57.19	43.46

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### 1.0 PURPOSE

Forecast models are tested with synthetic tsunami events covering a range of tsunami source locations. Testing is also done with selected historical tsunami events when available.

The purpose of forecast model testing is three-fold. The first objective is to assure that the results obtained with NOAA's tsunami forecast system, which has been released to the Tsunami Warning Centers for operational use, are identical to those obtained by the researcher during the development of the forecast model. The second objective is to test the forecast model for consistency, accuracy, time efficiency, and quality of results over a range of possible tsunami locations and magnitudes. The third objective is to identify bugs and issues in need of resolution by the researcher who developed the Forecast Model or by the forecast software development team before the next version release to NOAA's two Tsunami Warning Centers.

Local hardware and software applications, and tools familiar to the researcher(s), are used to run the Method of Splitting Tsunamis (MOST) model during the forecast model development. The test results presented in this report lend confidence that the model performs as developed and produces the same results when initiated within the forecast application in an operational setting as those produced by the researcher during the forecast model development. The test results assure those who rely on the Arecibo tsunami forecast model that consistent results are produced irrespective of system.

#### 2.0 TESTING PROCEDURE

The general procedure for forecast model testing is to run a set of synthetic tsunami scenarios through the forecast system application and compare the results with those obtained by the researcher during the forecast model development and presented in the Tsunami Forecast Model Report. Specific steps taken to test the model include:

- 1. Identification of testing scenarios, including the standard set of synthetic events and customized synthetic scenarios that may have been used by the researcher(s) in developing the forecast model.
- 2. Creation of new events to represent customized synthetic scenarios used by the researcher(s) in developing the forecast model, if any.
- 3. Submission of test model runs with the forecast system, and export of the results from A, B, and C grids, along with time series.
- 4. Recording applicable metadata, including the specific version of the forecast system used for testing.
- 5. Examination of forecast model results from the forecast system for instabilities in both time series and plot results.
- 6. Comparison of forecast model results obtained through the forecast system with those obtained during the forecast model development.
- 7. Summarization of results with specific mention of quality, consistency, and time efficiency.
- 8. Reporting of issues identified to modeler and forecast software development team.
- 9. Retesting the forecast models in the forecast system when reported issues have been addressed or explained.

Synthetic model runs were tested on a DELL PowerEdge R510 computer equipped with two Xeon E5670 processors at 2.93 Ghz, each with 12 MBytes of cache and 32GB memory. The processors are hex core and support hyperthreading, resulting in the computer performing as a 24 processor core machine. Additionally, the testing computer supports 10 Gigabit Ethernet for fast network connections. This computer configuration is similar or the same as the configurations of the computers installed at the Tsunami Warning Centers so the compute times should only vary slightly.

#### Results

The Arecibo forecast model was tested with NOAA's tsunami forecast system version 3.2.

The Arecibo, Puerto Rico forecast model was tested with three synthetic scenarios. Test results from the forecast system and comparisons with the results obtained during the forecast model development are shown numerically in Table 2 and graphically in Figures 1 to 3. The results show that the forecast model is stable and robust, with consistent and high quality results across geographically distributed tsunami sources and mega-event tsunami magnitudes. The model run time (wall clock time) was under 19 minutes for 8 hours of simulation time, and around 9 minutes for 4 hours. This run time is at the 10 minute run time for 4 hours of simulation time and satisfies time efficiency requirements.

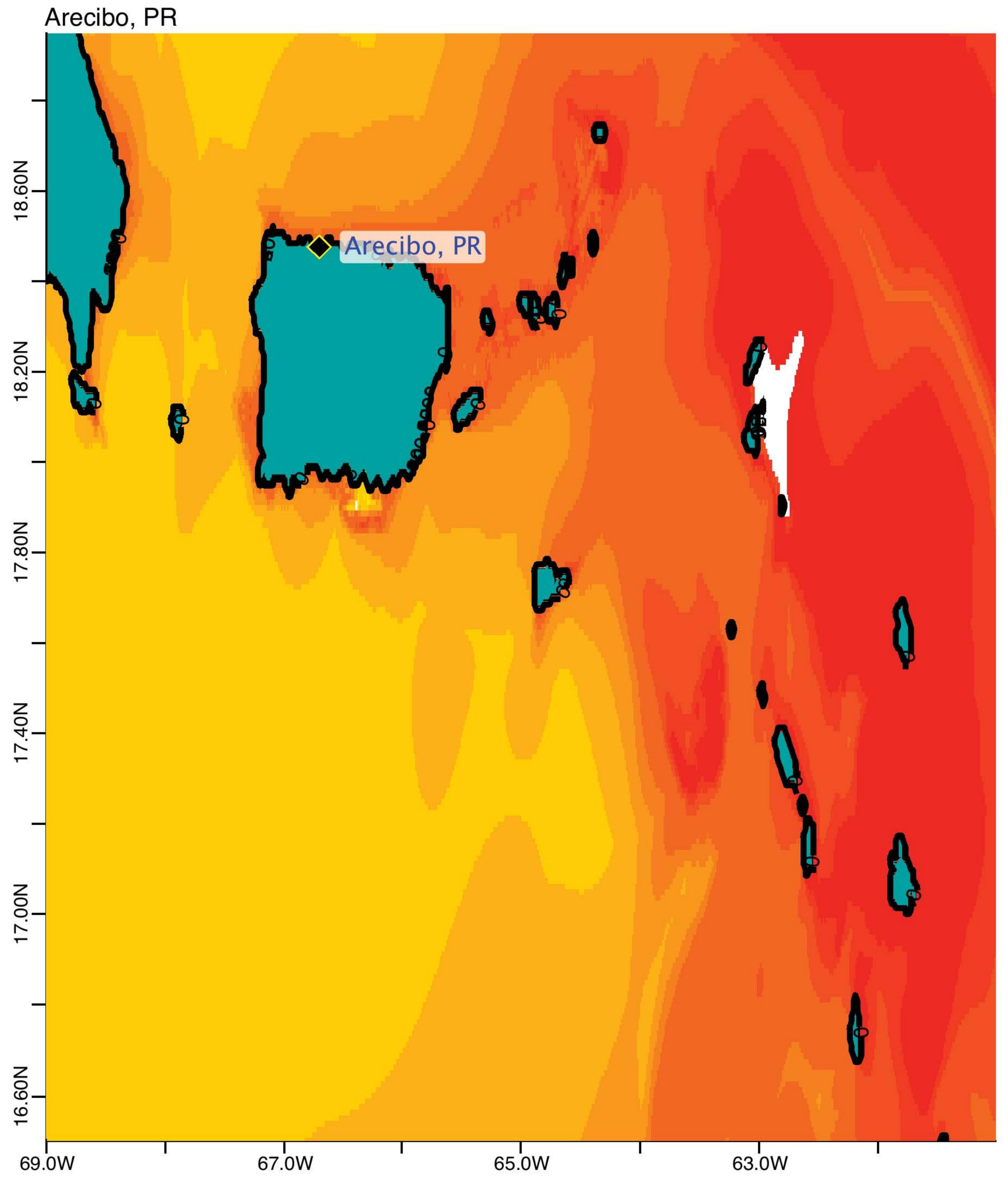
Three synthetic events were run on the Arecibo forecast model. The modeled scenarios were stable for all cases tested, with no instabilities or ringing. Results show that the largest modeled amplitude was 14.41 m and originated in the Caribbean (ATSZ 48-57) source. Amplitudes greater than 100 cm were recorded for the two of three test sources. The smallest signal of 14.4 cm was recorded for the far field South Sandwich Islands (SSSZ 1-10) source. Direct comparisons, of output from the forecast tool with results from available development synthetic events, demonstrated that the wave patterns are similar in shape, pattern and amplitude (the Caribbean (ATSZ 48-57) source has 1 difference and maximums differ by 11cm). The discrepancies are mainly caused by different propagation databases used to provide the boundary conditions for model runs. Developed in 2008, the forecast model report shows the Arecibo model results based on an old tsunami propagation database, while the SIFT testing results in Appendix C reflect the tsunami propagation database that was updated in December of 2011. It is known that the new propagation database will lead to improvement of the model results.

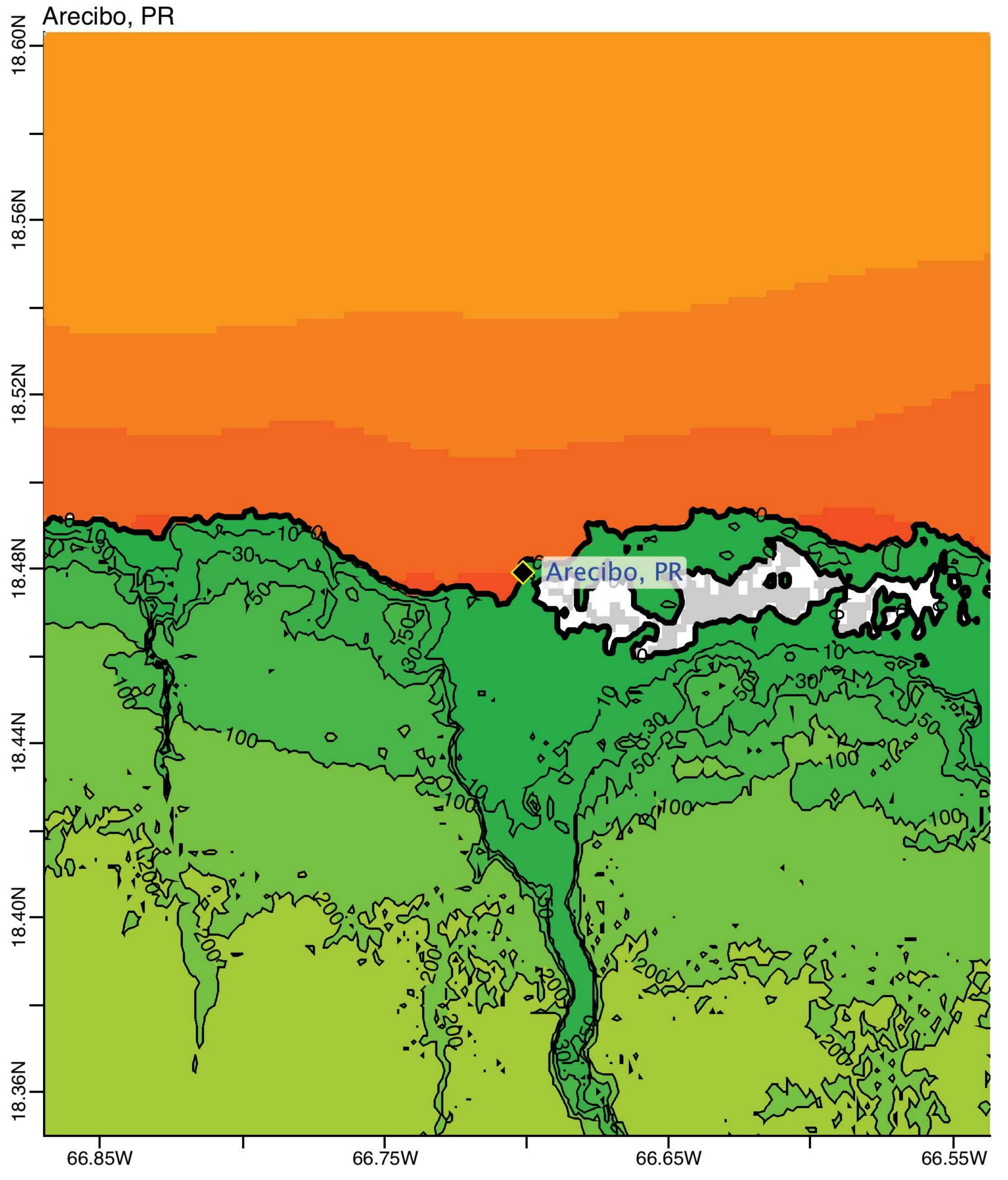
Table 1. Table of maximum and minimum amplitudes (cm) at the Daytona Beach, Florida warning point for synthetic and historical events tested using SIFT 3.2 and

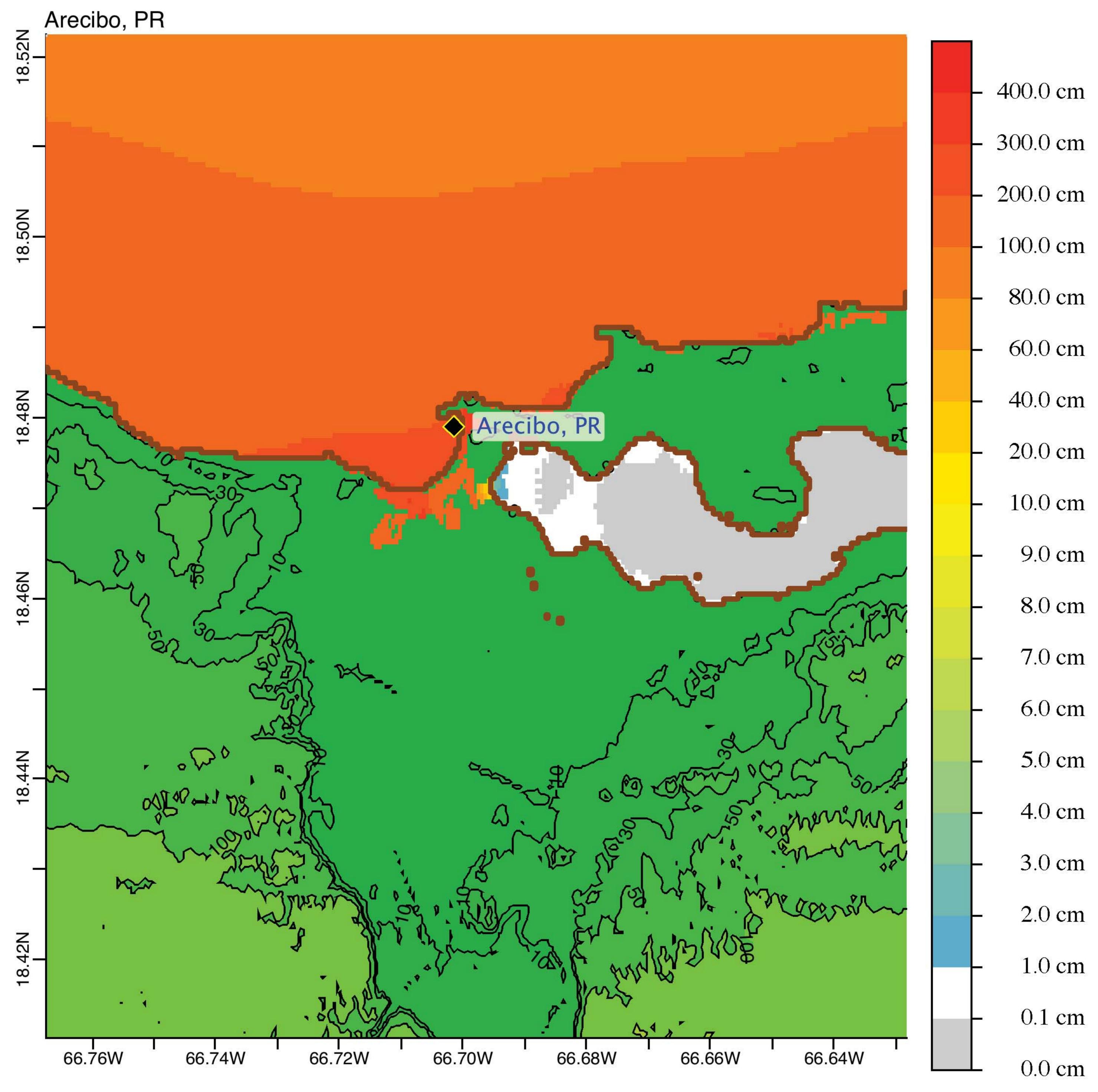
obtained during development.

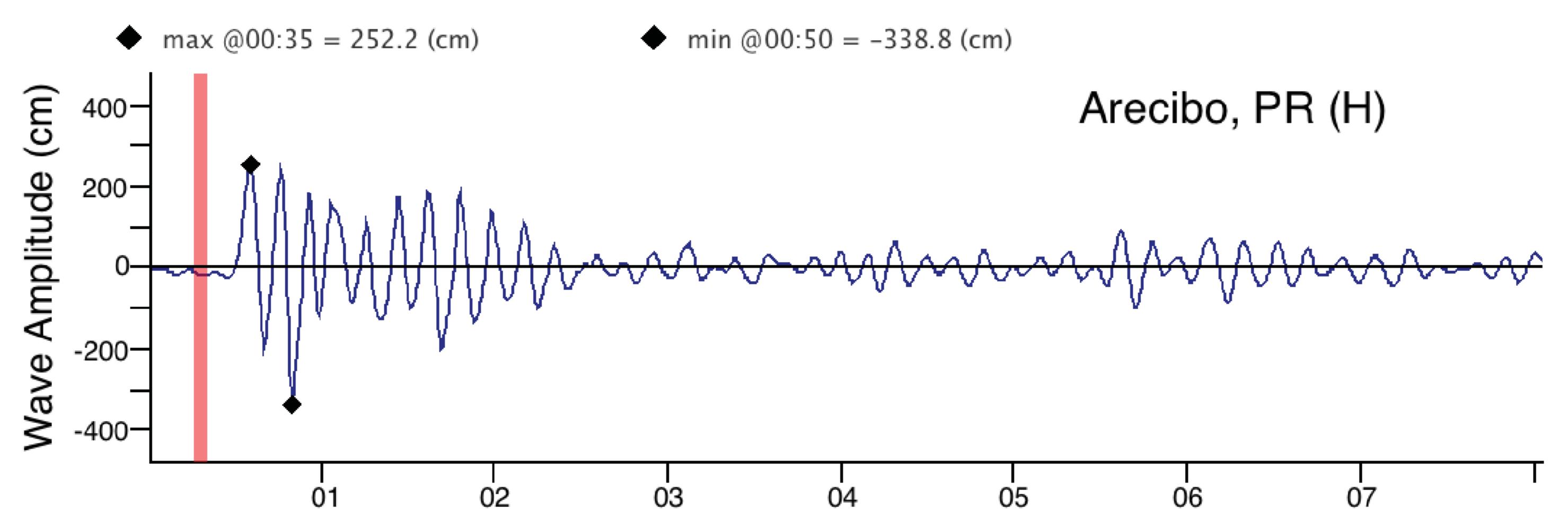
Scenario Name	Source Zone	Tsunami Source	α [m]	SIFT Max (cm)	Development Max (cm)	SIFT Min (cm)	Development Min (cm)	
Mega-tsunami Scenarios								
ATSZ 38-47	Caribbean	A38-A47, B38-B47	25	252.2	252	-338.8	-338	
ATSZ 48-57	Caribbean	A48-A57, B48-B57	25	1441.4	1430	-582.7	-583	
SSSZ 1-10	South Sandwich Islands	A1-A10, B1-B10	25	14.4	14	-14.6	-14	

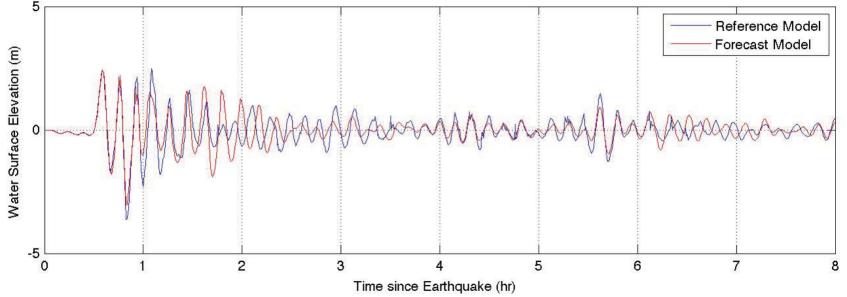
Model	Modeled T	'ime Wal	l Time 4-h	our time	Disk Space	e 12-hour Space
	[1	nrs]	[min]	[min]	[Gb]	[Gb]
LW2-atsz38-47.02	.IF_ARC 0	8.03	16.83	08.36	0.00	0.00
LW2-atsz48-57.02	.IF_ARC 0	8.03	18.15	09.04	0.00	0.00
LW2-sssz1-10.02.I	F_ARC 0	8.03	16.93	08.40	0.00	0.00

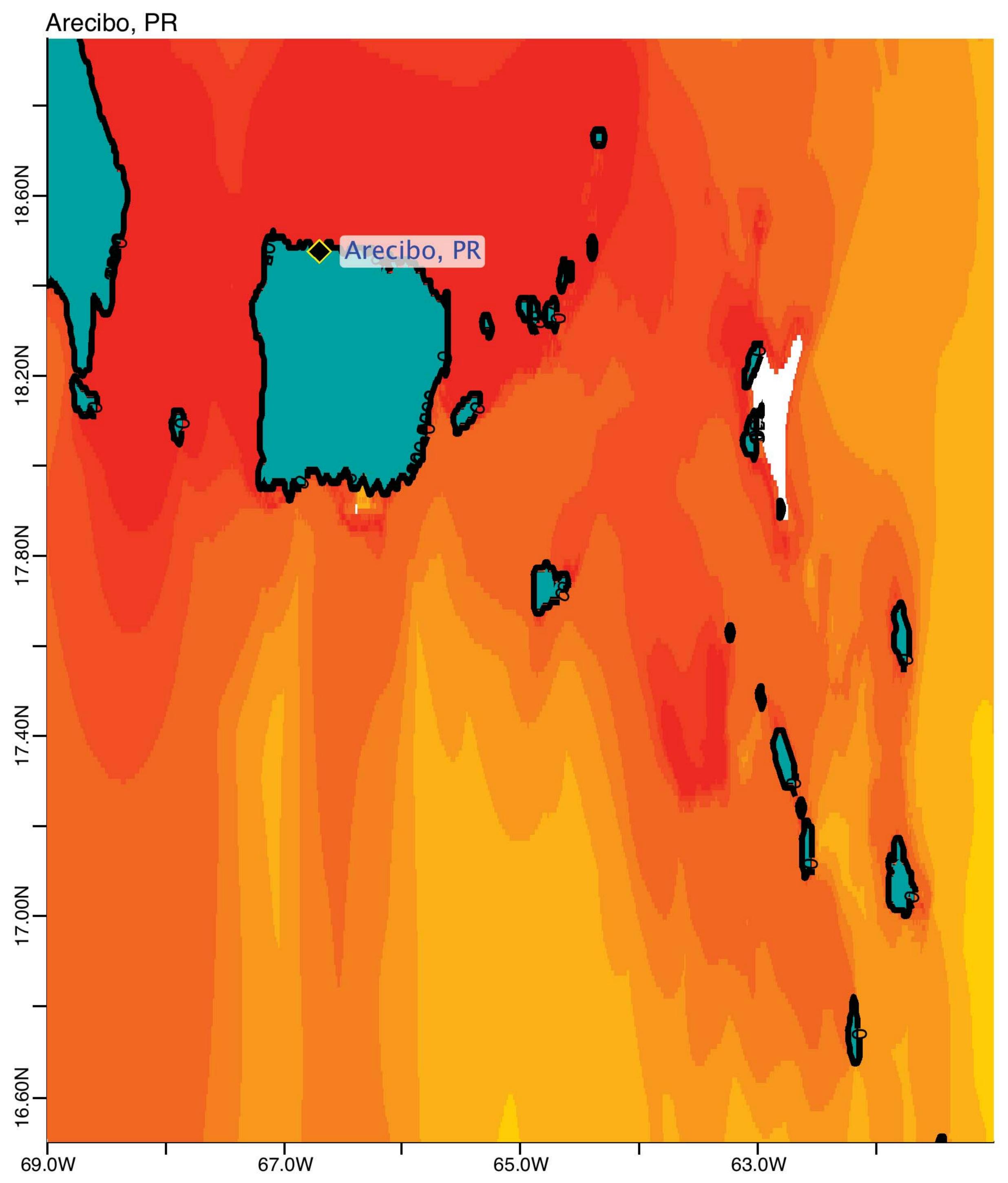


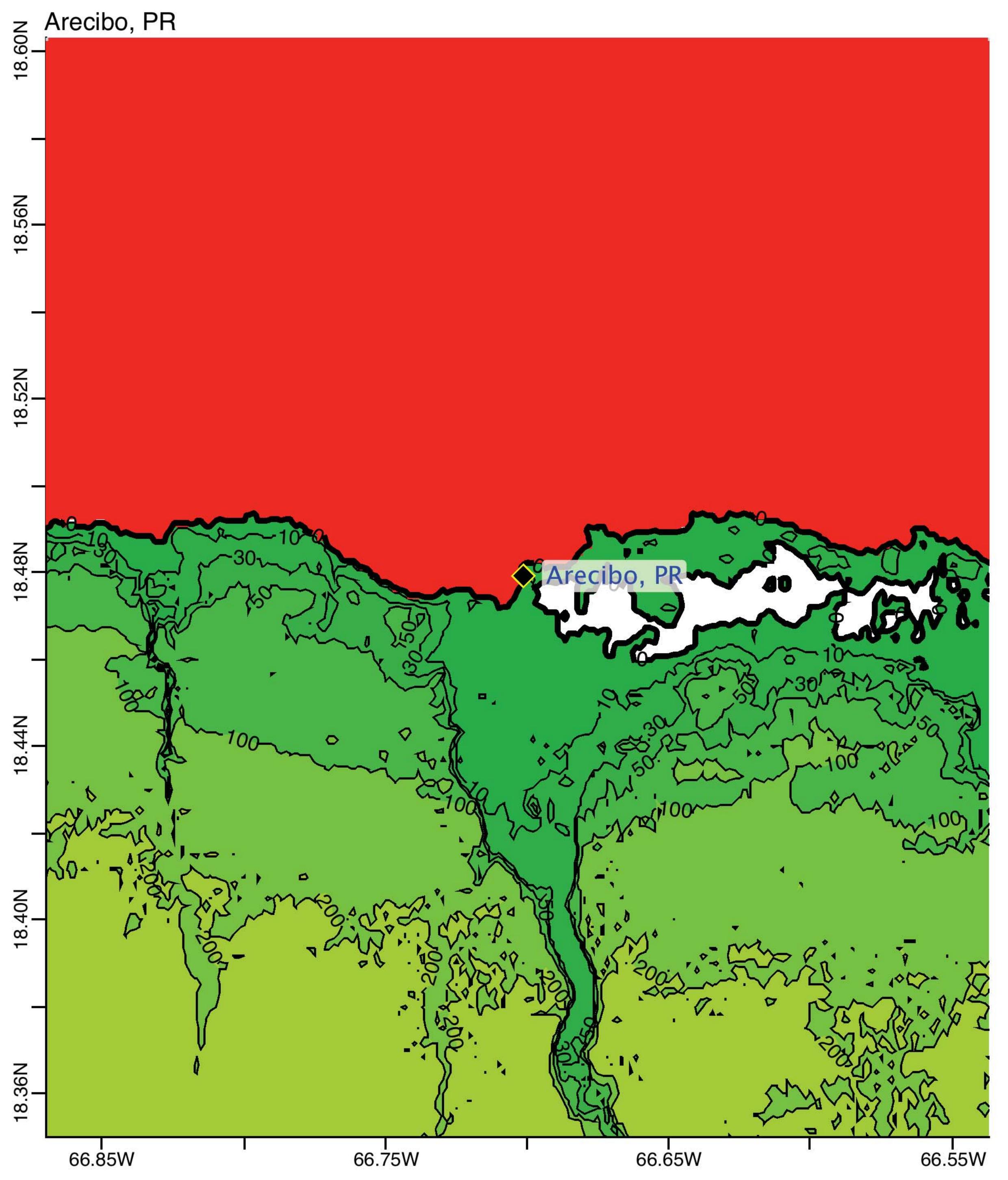


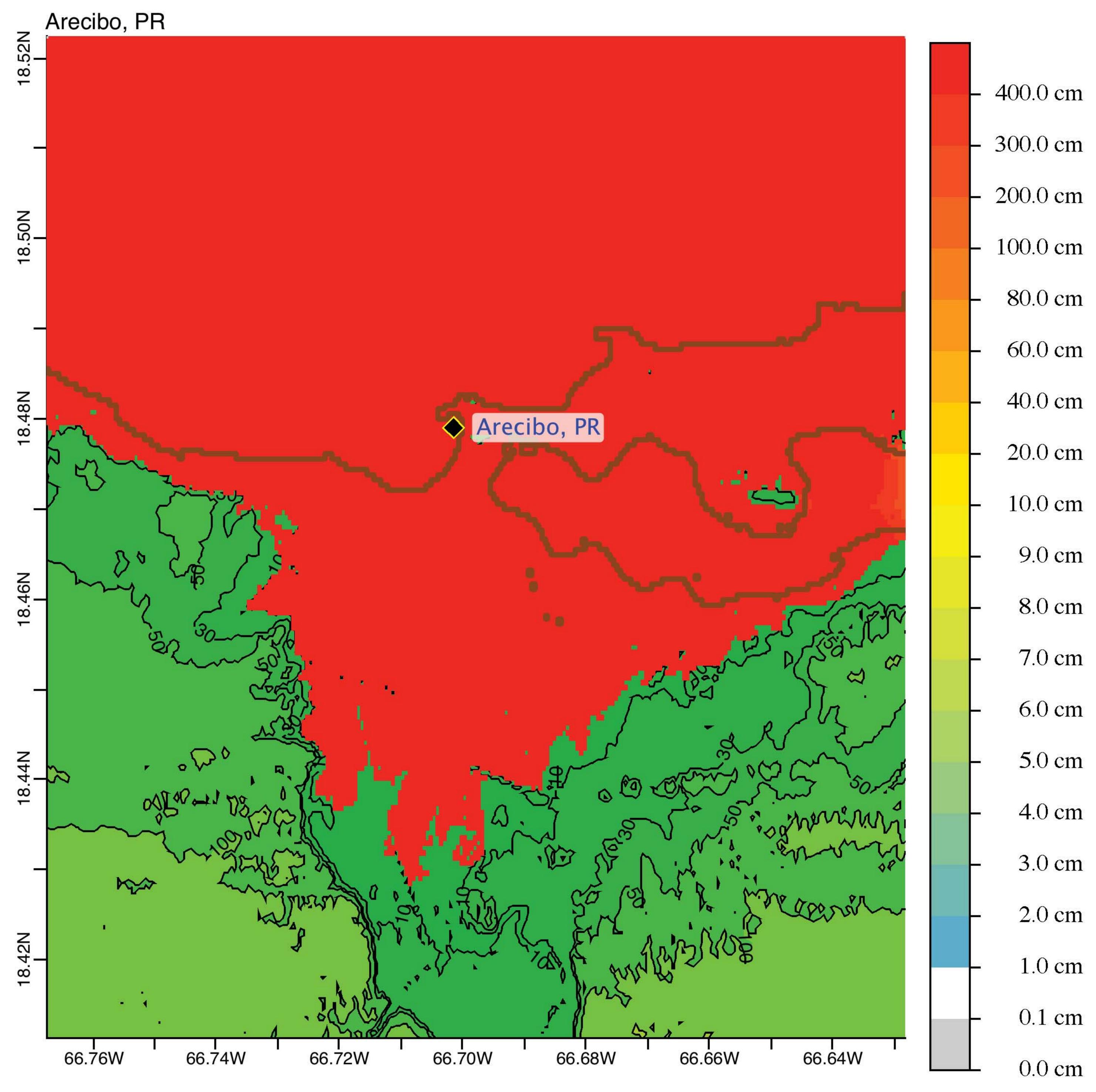


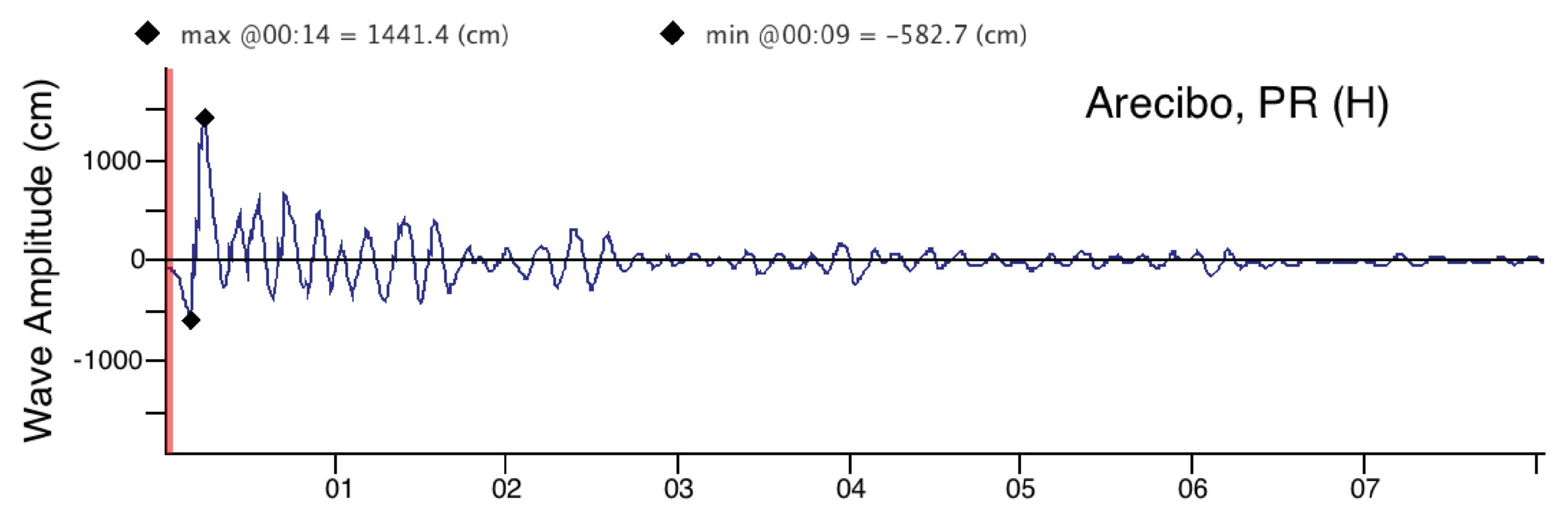


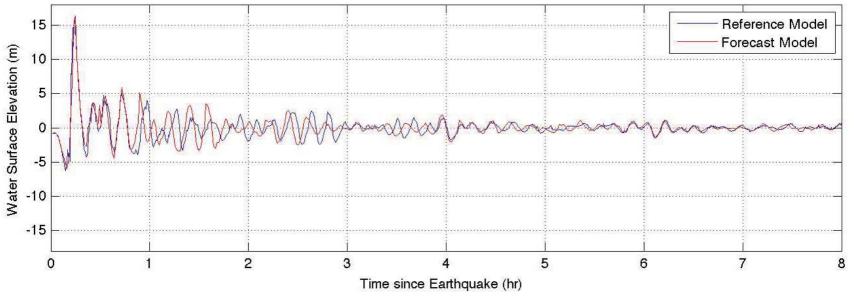


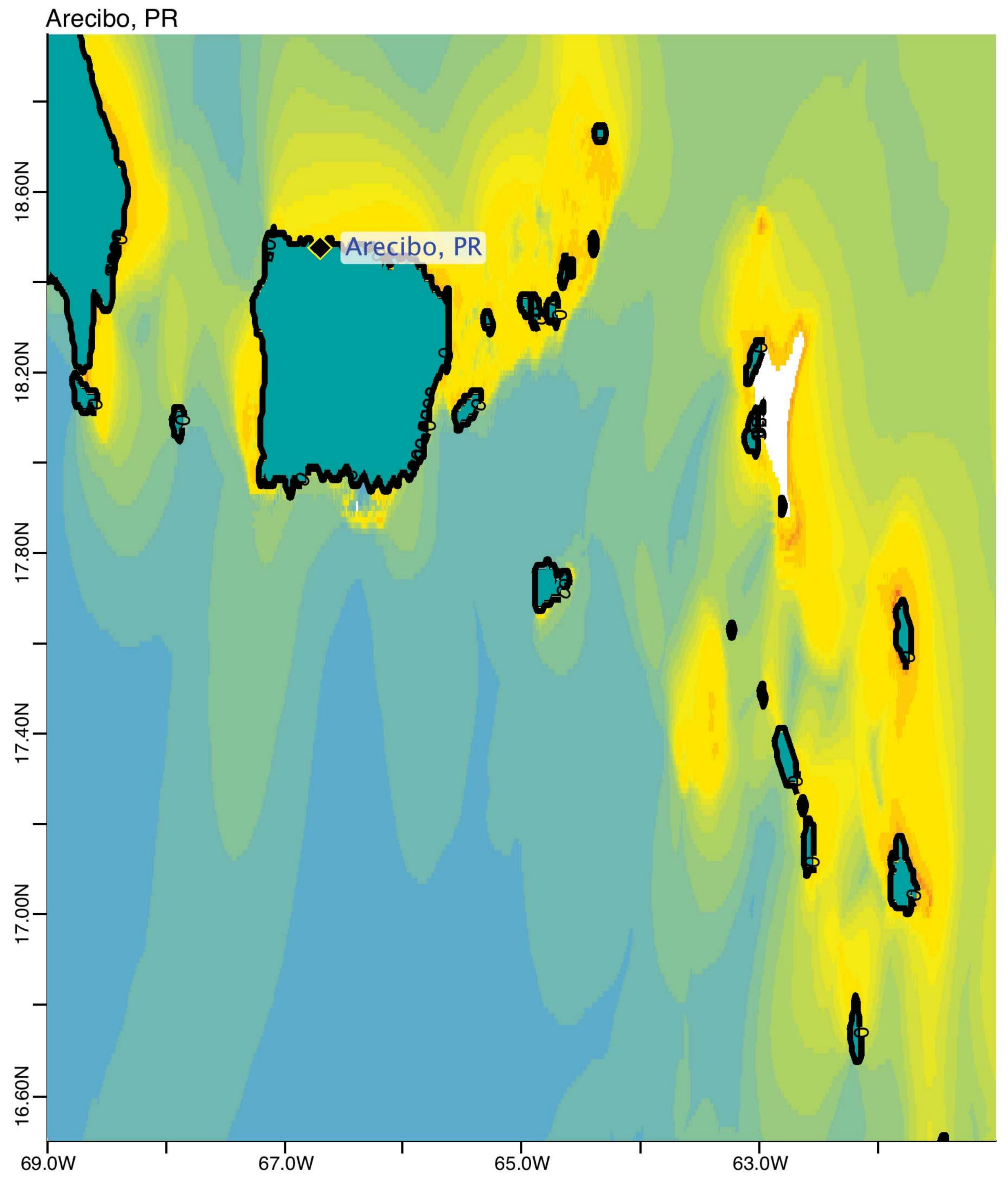


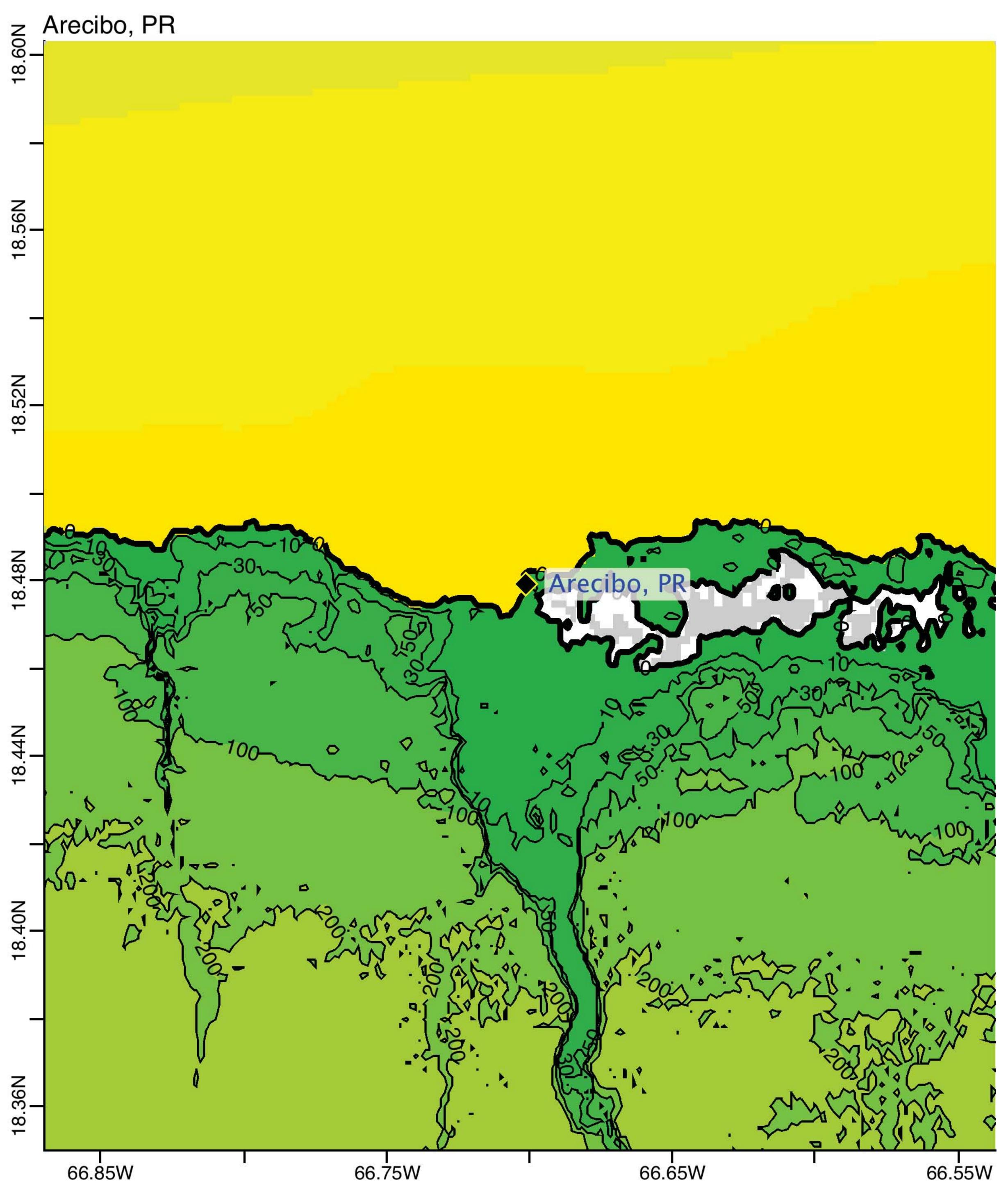


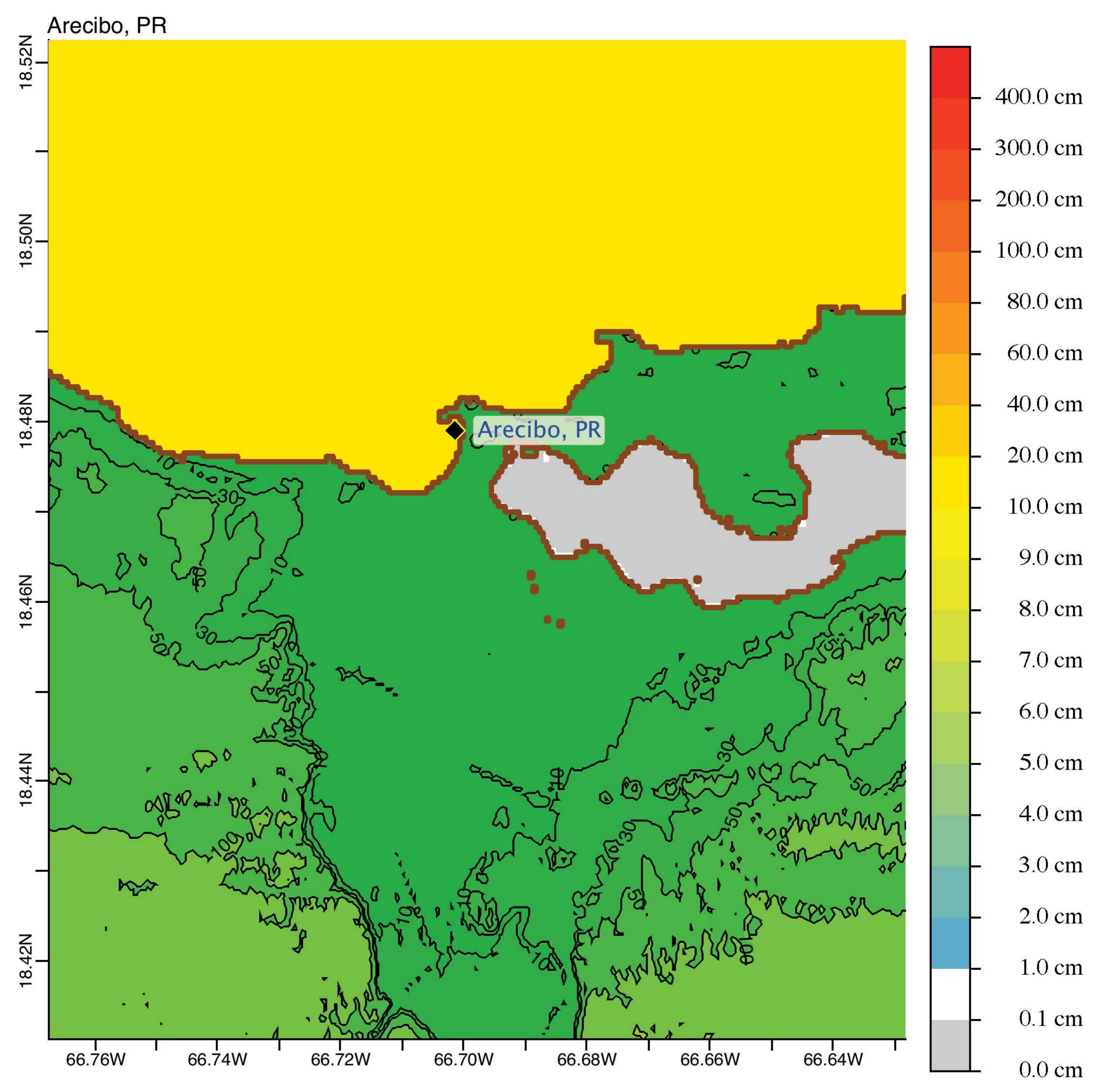


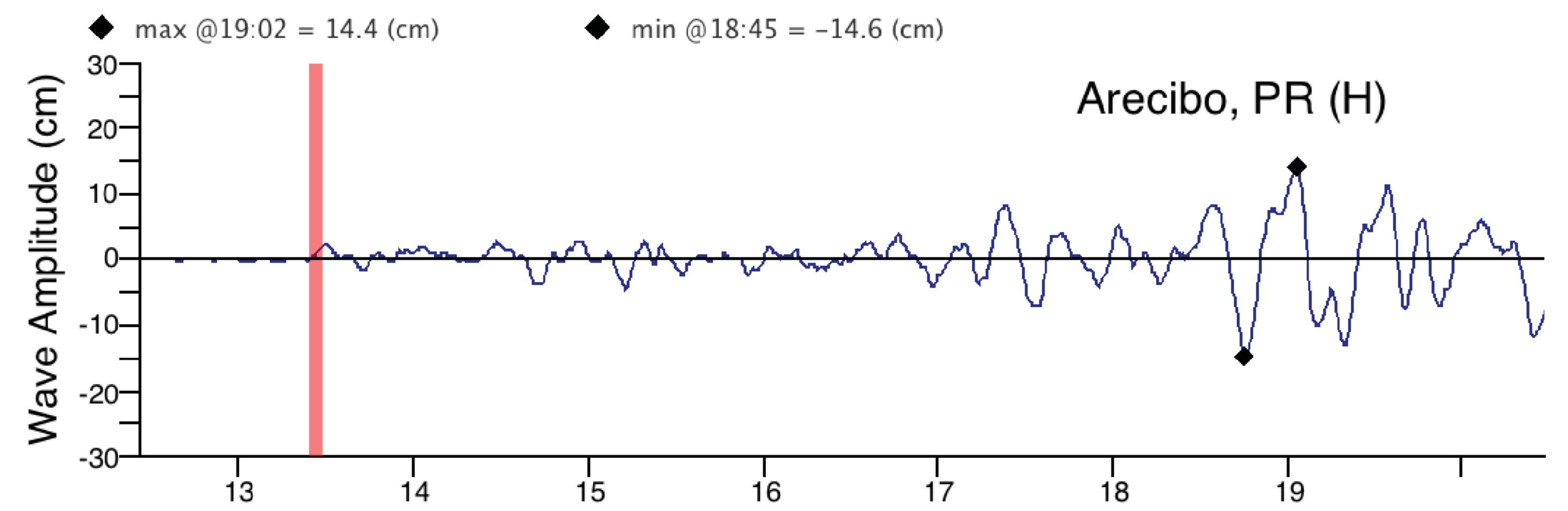


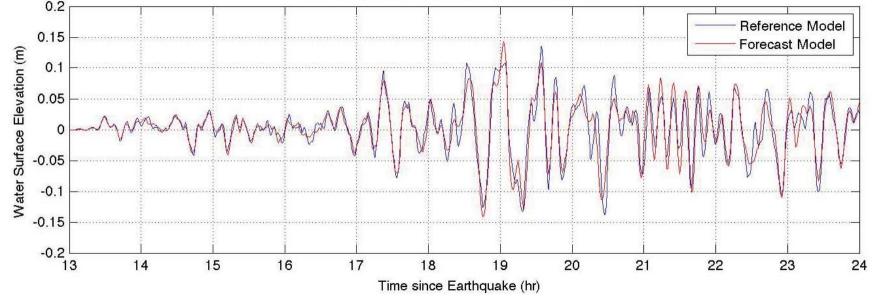












### Appendix D

